

Multiple Linear Regression Analysis of Pumps Performance in Water Pumping Plants

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Abstract. Energy use in water supply systems represents a consequent part of global energy consumption across all sectors. This consumption is expected to rise, due to the increasing demand and the recourse to unconventional water resources. Regarding water utilities, most of their operating costs are related to energy consumption, especially pumping systems consumption. In this context, the main objective of this study was to model accurately the energy consumption of pumping systems in order to optimize the whole water supply system, thus improving its efficiency, especially in the case of a limited renovation. For this purpose, Multiple Linear Regression was fitted to model the produced kWh/m^3 ratio according to the following parameters, active and reactive energies, the daily produced water volume, the power factor ($\text{Cos}\phi$), and the operating time of each pump. The final model describes accurately the consumption per cubic meter produced with R^2 square statistic reaching 0.91 and value standard error is close to 5% were found. Therefore, this model could be considered a good estimator for the calculated ratio, which was close to the experimental one. In addition, this approach considers the system's behavior while most of the comparable studies focus on the pump scheduling problem estimator for the calculated ratio which was close to the experimental one. In addition, this approach considers the real-time-data behavior while most of the comparable studies focus on the pump scheduling problem.

Key Words: Energy efficiency, multiple linear regression, pumping systems, water supply system.

37 **1. Introduction**

38 In the upcoming decades, water demand is forecasted to significantly increase up to
39 35% in 2050 (UN-Water 2020). Therefore, energy needs that are related to the water
40 pumping and distribution processes could contribute to the expected increase in
41 energy demand (EIA 2019). Indeed, several studies have concluded that the energy
42 consumption related to these process accounts for 7% of the total energy used across
43 the globe (Coelho et al., 2014). His share is expected to get bigger due to the
44 increasing distances between resources and populations, especially in water-scarce
45 countries, and the growing consumption per capita due to the industrialization and
46 improvement of living standards.

47 To reach the sixth Sustainable Development Goal (SDG6) that aims to
48 generalize the access to drinking water supply, the water production cost mustn't
49 impact its price which should stay affordable to the population. Therefore,
50 production costs should be reduced via the control of energy consumption which is
51 typically the largest marginal cost for the production (Helena et al., 2017).

52 Pumping processes consume the largest fraction of total energy (Plappally and
53 Lienhard, 2012). The pumps consumption often presents 80% to 90% of the total
54 energy consumption (Sarbu, 2016). However, this consumption may depend on
55 many factors such as surface water or ground water, transport differences, flat or
56 mountain regions, etc (Rothausen and Conway, 2011) (Plappally and Lienhard,
57 2012). Thus, by achieving energy efficiency improvements measures, we may
58 reduce this consumption by 25% (Moreira, et al., 2013). In this context, few studies
59 were interested in modeling pumping systems and evaluated the influence of
60 parameters such as the aging of the components, which can reduce the performance
61 of the pump by up to 12% (Durmus, et al., 2008).

62 The improvement of the efficiency of the pumping has always been an
63 important part. Since many specific factors impact the overall energy efficiency of a
64 water pumping system such as surface water or ground water, transport differences,
65 flat or mountain region... One important factor is the operating point which should
66 be as close as possible to the maximum energy efficiency region (Caravetta, et al.,

67 2020). Another factor is the age of the system, especially the pumps which can lose
68 1.5% of their efficiency every year (Zhou et al., 2021). Many attempts have been
69 made to address the subject of pumping optimization using different approaches to
70 optimize either energy consumption or the overall cost of energy. To optimize the
71 energy consumption, a model based on ant colony was utilized (Ostfeld and
72 Tabaltzev, 2008) to provide an effective model that minimizes the design and the
73 operating costs. This model act on parameters such as: the diameters of the pipes,
74 the pumping station's maximum power, and the tank's storage. Another work
75 targeting the minimization of energy consumption (Giustolisi O et al., 2012) used a
76 multiobjective strategy to minimize losses by controlling pressure in the water
77 distribution system and thus minimizing the energy consumption.

78 On the other hand, various studies have focused on optimizing the operation of
79 the existing water systems by using deterministic methods such as Dynamic
80 Programming (Fallside and Perry, 1975) which worked on minimizing the energy
81 cost by load shifting using a hierarchical optimization to reduce the problem to 10
82 control parameters. Given the difficulty of the deterministic approach, different
83 metaheuristic methods were developed, the widely used among them is Genetic
84 Algorithms (Wu et al., 2014) which used evolutionary computation to maximize the
85 efficiency of a system consisting of 2 pumps. Although these efforts employ
86 evolutionary optimization techniques. However, in literature, particular attention has
87 been paid to the applicability of linear regression (Puleo et al., 2014) and multiple
88 linear regression (Adamowski et al., 2012) to the pumping scheduling optimization
89 problem.

90 This work introduces a method of using multiple regression method to analyze
91 the key factors affecting the efficiency of the pumping for drinking water
92 production. Hence, this paper presents the results targets the pumping system of the
93 Bab Louta drinking water production located in the province of Taza, Morocco. In
94 this perspective, a multiple linear regression (MLR) was fitted to model the
95 produced kWh/m³ ratio according to the input parameters by using real-Time-data

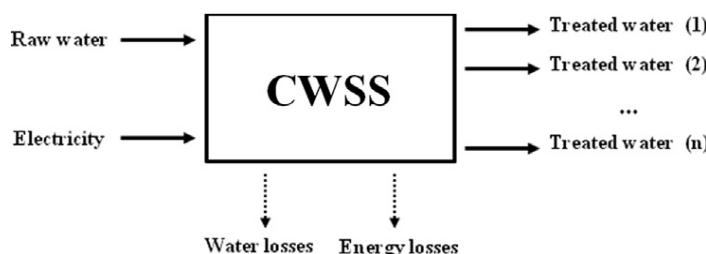
96 such as the active energy and reactive energy consumed by the pumping station, the
97 daily produced volume, the power factor and the pump operating time.

98

99 **2. Materials and methods**

100 Conventional water supply systems (WSS) consist of sets of structures and facilities
101 providing products with a suitable quantity and quality for domestic and industrial
102 use (Luna et al., 2019). To develop energy and hydraulic model, WSS systems
103 should be evaluated in terms of mass and energy (Figure 1).

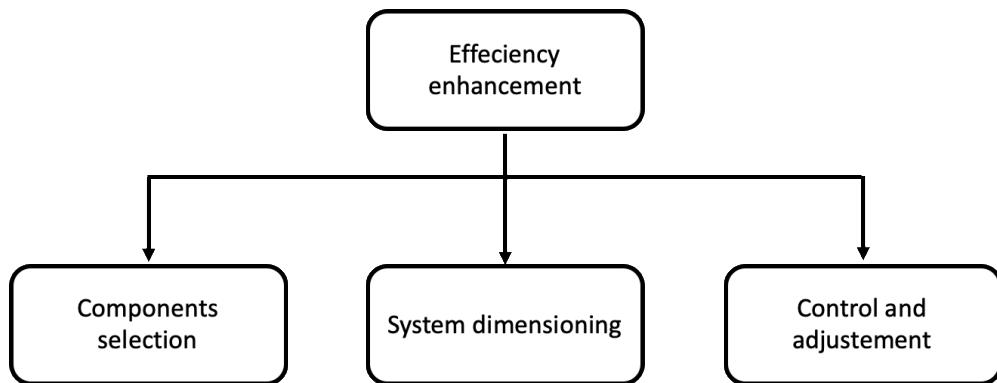
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105

106 **Figure 1:** Schematic diagram of the energy and hydraulic flows in a WSS (Vilanova, et al.,
107 2014).

108 There are various methods to enhance energy efficiency in WSS. These methods
109 are ranging from leakages control through simple monitoring operations to massive
110 investments by reviewing the design of the infrastructures, equipment upgrade,
111 pump system optimization, and real-time control. These Methods were classified
112 into 3 major sub-categories is shown in Figure 2 (Shankar, et al., 2016). These
113 factors affecting system efficiency, and formulate targeted improvement plans.



114

115 **Figure 2:** Scheme of the main factors affecting efficiency enhancement opportunities in
 116 WSS.

117 2.1 Study area and description of the drinking water production system

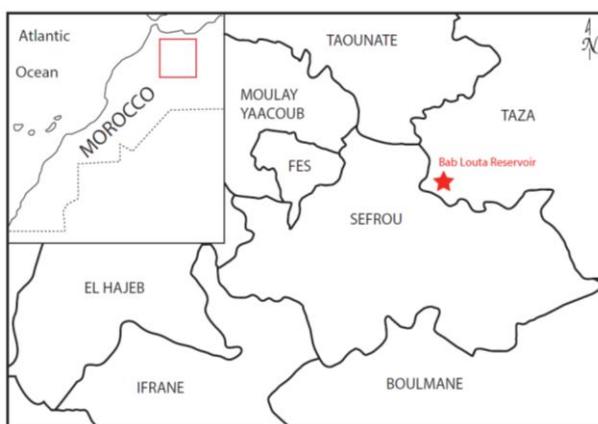
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119 The province of Taza is located in the center North of Morocco and it is one of the 9
 120 provinces of the region of Fez-Meknes with a population of roughly 530 000
 121 inhabitants (Morocco 2014). The water treatment plant of Tahla provides a large
 122 population of the province, mainly the urban areas. It is situated 60 km from the city
 123 of Taza. The plant treats the raw water of the Bab Louta reservoir.

124

125 The production system consists of a pumping station SP0 for raw water, a water
 126 treatment plant then another pumping station of SP3 to reach the city of Taza, which
 is the chief town of the province.

127



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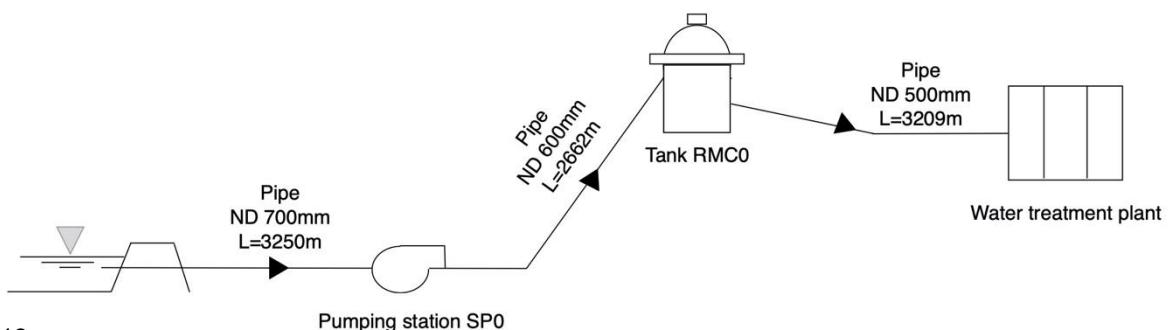
129 **Figure 3:** Location of the Bab Louta reservoir.

130 2.2 Description of the pumping station

131

132 The pumping station SP0 is located about 3km from the reservoir. It is responsible
133 for overcoming the difference in altitude between the raw water intake and the water
134 treatment plant. The water is taken by gravitation from the reservoir to the pumping
135 station SP0 through a pipe of a nominal diameter (ND) of 700 mm which converge
136 to a diameter of 500 mm just before reaching the SP0. Then, the water is pumped
137 through a pipe of a nominal diameter of 600 mm to a tank destined to provide the
138 water treatment plant with raw water, it is called RMC0 and having a capacity of
139 1000 m³, which provides the water treatment plant with raw water through a pipe of
140 a nominal diameter of 500 mm (ONEE 2019).

141

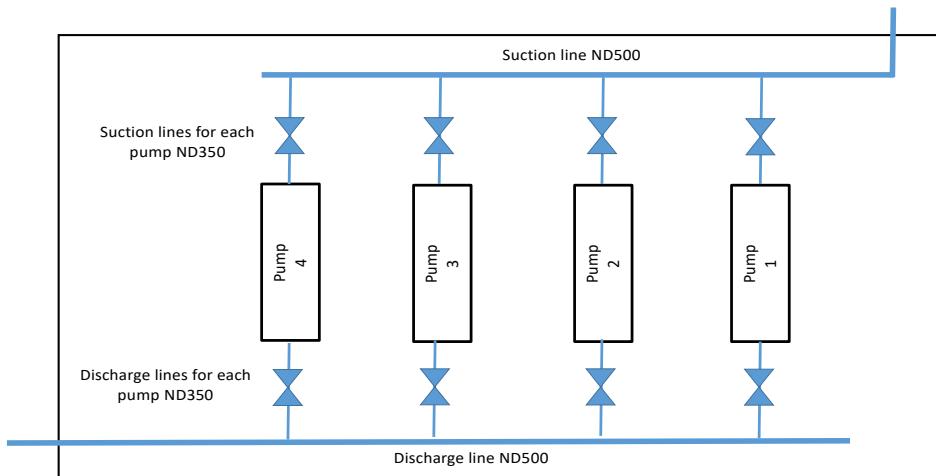


142 Bab Louta reservoir

143 **Figure 4:** A simplified example of a water treatment plant with water source (Bab Louta
144 reservoir), pumping station (SP0) and one water tank (RMC0).

145 The pumping station, the object of the current study, is situated at an altitude of
146 498.20 m and tank RMC0 is situated at an altitude of 737.80 m. SP0 consists of four
147 pumps (Figure 5) with a flow of 457 m³/h each and a manometric pressure of 209 m.
148 They are manufactured by the company HIDROTECAR powered by an electric
149 motor which is manufactured by LEROY SOMER with a nominal power of 455 kW
150 (ONEE, 2019).

151



152
153 **Figure 5:** Hydromechanical scheme of the pumping station SP0.
154

155 2.3 Experimental procedure
156

157 To obtain a reliable model of our system, measurements of the key parameters
158 influencing this system were conducted. These measurements were taken in the
159 period between January 2015 and December 2018 daily for the parameters. Based
160 on the above analysis, a total of eight factors affecting the efficiency of the pumping
161 for drinking water production are selected, namely:

- 162 • P: the active energy consumed by the pumping station (measured by a
163 wattmeter),
- 164 • Q: the reactive energy consumed by the pumping station (measured by a
165 wattmeter),
- 166 • V: the daily produced volume (measured by an electromagnetic
167 flowmeter),
- 168 • $\text{Cos}\phi$: the power factor,
- 169 • HMG1: the pump operating time “1”,
- 170 • HMG2: the pump operating time “2”,
- 171 • HMG3: the pump operating time “3”,
- 172 • HMG4: the pump operating time “4”.

173 This study investigates the impact of these several independents variables on the
174 energy use of a drinking water production. The starting from these parameters, the
175 principal component analysis is performed, and the comprehensive evaluation
176 function equation and the regression equation can be obtained, respective.

177

178 **2.4 Modelling**

179
180 This study aimed to use Multiple Linear Regression (MLR) analysis to predict an
181 output from a range of inputs. MLR model with multiple input variables can be
182 expressed as follows (Longo et al., 2016):

183

$$184 \quad Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \dots + \beta_n X_n + \varepsilon \quad \text{Eq 1}$$

185

186 Where, Y is the output variable, β_i are the regression parameters, X_i are the input
187 variables ($i = 1, \dots, n$) and ε is the random error.

188

189 In order to assess the influence of the included parameters on the cubic meters ratio
190 produced by the pumping station, the following parameters were considered: the
191 active energy (E_p), the reactive energy (E_q), the daily produced volume (V), the
192 power factor ($\text{Cos}\varphi$), and the operating time of each pump (HMG_i). Therefore, the
193 principal parameter analysis is used to establish the evaluation model to achieve
194 more objective and accurate analysis.

195 The effect of eight variables on the produced Kwh/m^3 ratio was evaluated. Of
196 note, 1388 experiments were conducted during 4 years. The set of analysis data is
197 shown in Table 1.

198

199 **Table 1:** Problem characteristics

Objective of the study	The effect of the variables on the ratio KWh/m^3
Number of Variables	8
Number of experiments	1388
Number of the coefficients	8
Number of responses	1

200

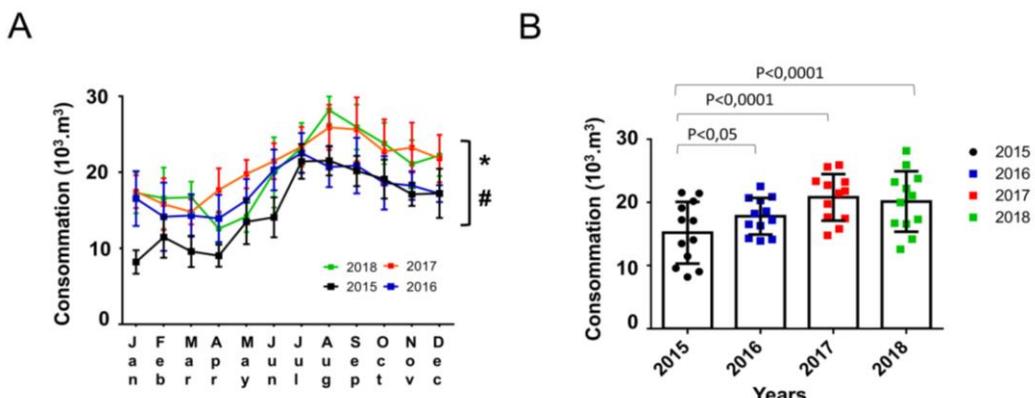
201 **Table 2:** Measurements summary of the mean and standard deviation during period
 202 2015 and 2018

	E_p (kWh)	E_Q (kVar)	$\text{Cos}\varphi$	Production (m^3)	HMG1 (m)	HMG2 (m)	HMG3 (m)	HMG4 (m)	Ratio (kWh/m^3)
Mean	14 837.47	8 339.58	0.87	18 181.40	7.95	7.63	10.43	9.01	0.82
Standard deviation	9 158.63	8 529.85	0.05	5 081.13	8.90	5.88	11.51	8.85	0.43

203

204 The descriptive statistics of the pumping station parameters under study are given
 205 in Table 2. It provides a summary of the mean and standard deviation values of eight
 206 measured parameters during 4 years. In this case, generally for each year, the mean
 207 direct production about 18181 m^3 related active energy of 14837 kWh with the
 208 operating time of each pump (HMG_i) to range between 8 and 10 m. Figure 6 displays
 209 the real water consummation versus the month and year that is measured over four
 210 years.

211



212

213 **Figure 6:** Representation the dataset collected of the variation of the consumptions of water
 214 versus the months during period 2015 and 2018, (A) consumption variation through the
 215 months (*: $P<0.05$, consumption variation through the years; #: $P<0.05$, consumption
 216 variation through the months), (B) consumption variation through the years ($P<0.05$ is
 217 considered as statistically significant. Each point represents the consumption average of a
 218 given month during the year).

219 The dataset collected of the water production across the year for each year from
220 2015 to 2018 presented in figure 6-A, and it the trend shows that clearly
221 demonstrates a higher production which reflects a higher consumption of water
222 during the summer months in province of Taza. On the other hand, figure 6-B shows
223 the evolution of the production through the years 2015 to 2018 and it has also the
224 same increasing trend due to the continuous commissioning of new networks
225 leading to a growing number of consumers.

226 It can be seen from Table 1, 2 and Figure 6 that the original data has large
227 differences and many influencing factors, and it is difficult to conduct
228 comprehensive and systematic analysis by conventional methods. Therefore, the
229 MLR analysis method is used to establish the evaluation model to achieve more
230 objective and accurate analysis.

231

232 **3. Results and discussion**

233 3.1 Statistical interpretation

234
235 The correlation coefficients shown in a matrix (Table 3) are the results of statistical
236 analyses for possible relationships between different parameters monitored. It was
237 found that the studied variables are strongly correlated:

- 238 • The active energy consumed by the pumping station was dependent on the
239 production, reactive energy, pumps operating hours (4;1), power factor
240 ($\text{Cos}\varphi$), HMG2, and HMG3 respectively.
- 241 • The reactive energy consumed is highly was dependents on the production,
242 active energy, $\text{Cos}\varphi$, pumps operating hours (4;1;2;3) respectively.
- 243 • $\text{Cos}\varphi$ was dependent on the reactive energy, the production, active energy,
244 pumps operating hours (4;1;3;2) respectively.
- 245 • Production was dependent on the active energy, the reactive energy pumps
246 operating hours (4;1;2;3).

Table 3: Correlation matrix of water pumping station parameters

Variable	Correlations (MATRIX CR without outliers) Marked correlations are significant at P< 0.05000 N=1388 (Case wise deletion of missing data)										
	Means	Std. Dev.	P	Q	Cosφ	Prod	HMG1	HMG2	HMG3	HMG4	Ratio
P	-0.022423	0.487229	1.000000	0.883071	-0.190305	0.939746	0.333340	0.202424	0.169873	0.625872	0.463030
Q	-0.027636	0.345041	0.883071	1.000000	-0.585775	0.883506	0.332525	0.170169	0.170505	0.612964	0.298339
Cosφ	0.026763	0.761882	-0.190305	-0.585775	1.000000	0.316528	-0.197066	0.024943	-0.076562	-0.271961	0.193819
prod	0.000741	0.973866	0.939746	0.883506	-0.316528	1.000000	0.340309	0.222533	0.175107	0.613597	0.150594
HMG1	-0.001400	1.002171	0.333340	0.332525	-0.197066	0.340309	1.000000	-0.164919	-0.016355	0.236341	0.111733
HMG2	-0.001865	0.998758	0.202424	0.170169	0.024943	0.222533	-0.164919	1.000000	-0.086627	-0.141591	0.006575
HMG3	0.001362	1.003257	0.169873	0.170505	-0.076562	0.175107	-0.016355	-0.086627	1.000000	0.074751	0.036371
HMG4	-0.017745	0.708400	0.625872	0.612964	-0.271961	0.613597	0.236341	-0.141591	0.074751	1.000000	0.0257315
Ratio	-0.051987	0.197427	0.463030	0.298339	0.193819	0.150594	0.111733	0.006575	0.036371	0.0257315	1.000000

248 Therefore, it is necessary to comprehensively consider the efficiency of the
 249 pumping unit, summarized in table 4. Table 4 lists the standardized regression
 250 coefficients and regression coefficients of various factors on system efficiency. The
 251 standardized regression coefficients can be used to construct the multiple
 252 Regression equation. ‘T-test’ shows that the probability of rejection of truth for all
 253 factors except the constant term is less than 0.05, indicating that the above
 254 regression factors have significant effects on the dependent variables. Moreover, it
 255 was concluded that the factors influencing the kWh/m³ ratio in descending order
 256 are:

- 257 • Ratio is positively correlated with the active energy consumed by the
 258 pumps;
- 259 • Ratio is negatively correlated with the production;
- 260 • Ratio is positively correlated with Cosφ;
- 261 • Ratio is negatively correlated with the reactive energy consumed by the
 262 pumps;
- 263 • Ratio is positively correlated with the operating hours of pumps 1 and 4.

264

265 **Table 4:** Regression summary for dependent variable

N=1388	Standardized regression coefficient (b*)	Standard error of b*	Regression coefficient (b)	Standard error of b	T-test (1379)
Intercept			-0.026073	0.001608	-16.2112
Prod	-2.52837	0.026164	-0.512563	0.005304	-96.6366
HMG ₁	0.02116	0.008985	0.004168	0.001770	2.3546
HMG ₂	0.01693	0.009327	0.003346	0.001844	1.8150
HMG ₃	-0.00080	0.008299	-0.000157	0.001633	-0.0960
HMG ₄	0.04287	0.011275	0.011948	0.003142	3.8023
P	2.85701	0.043662	1.157669	0.017692	65.4347
Q	-0.08315	0.040932	-0.047577	0.023421	-2.0314
Cosφ	0.09614	0.020445	-0.024913	0.005298	-4.7023

266

267

268 The variance analysis of data in Table 5 has shown that eight variables are
 269 significant which are Prod, HMG1, HMG2, HMG3, HMG4, P, Q and Cosφ. It can
 270 be observed that the regression mean squares was superior to the residual mean
 271 squares, the Fischer value is very high and the p-value is strictly tended towards
 272 zero. Hence, the variance analysis result so all meet the regression requirements.
 273 Besides as shown in Table 6 that, the R-square and Adjusted R-square statistic of
 274 this model reaching 0.91 were found, which can reflect the good degree of influence
 275 of various factors on model. From the error analysis, it can be seen that the value
 276 standard error estimate is close to 0.05 (5%), thus error value is within a reasonable
 277 interval, and the regression equation is statistically significant. In view of these
 278 results, we can say that the parameters studied are highly variable in the research
 279 area, thus, they also confirm the performance of the developed model.

280

281 **Table 5:** Analysis of Variance for MLR Model

Effect	Analysis of Variance; DV: Ratio				
	Sums of Squares	df	Mean Squares	F	p-value
Regression	49.31283	8	6.164104	1790.044	0.00
Residual	4.74865	1379	0.003444		
Total	54.06149				

282

283 **Table 6:** Statistical evaluation of model

Statistic	Value
R	0.95507172
R ²	0.91216198
Adjusted R ²	0.9116524
Fischer (8.1379)	1790
p-value	0.00
Standard error of estimate	0.0586817579

284

285 Based on this presented Statistical data analysis, the following set of the
 286 parameters in the standardized regression equation are the data after standardized
 287 processing is proposed in the final model expressed by the equation below:

288
$$R_{ratio} = 2.85701 P - 2.52837 \text{ Prod} - 0.08315 Q + 0.09614 \text{ Cos}\varphi + 0.02116 \text{ HMG1} +$$

 289
$$0.01693 \text{ HMG2} - 0.00080 \text{ HMG3} + 0.04287 \text{ HMG4.} \quad \text{Eq 2}$$

290 Where, P-active energy consumed by the pumping station; Prod-production volume;
291 Q-reactive energy consumed by the pumping station; Cosφ-power factor; HMG_i-
292 pump operating time (i=1;2;3,4).

293 The regression equation obtained indicating that the above regression factors have
294 significant effects on the dependent variables.

295
296 3.2 Technical Interpretations
297

298 From this analysis, this study concluded that in order to improve the ratio per
299 produced cubic meter, a reduction of the active energy consumed by the pumps
300 should be considered. As the function point of the pumps is already set by the
301 system characteristics, only active energy could be reduced by the improvement of
302 the pumps efficiency.

303 The ratio is negatively correlated with production means; i.e., there is an
304 economy of scale. It means the most the production increases the least the ratio is.

305 The operating hours of the pumps 1 and 4 are positively correlated, which means
306 that more these pumps are used higher more the ratio is higher. Therefore, it is
307 recommended to use the pump 3, and if there is an operation of renovation of the
308 pumping station, it is recommended to start with upgrading the pumps 1 and 4. In
309 the event of a new investment, the company can increase the capacity of the RMC0
310 storage tank which, according to the model, will decrease the significantly the ration
311 and also allows a load shifting to the off-peak hours.

312 A regression analysis was performed, which identified the quantitative
313 relationships between input parameters and energy consumption ratio per cubic
314 meter water, involved in a water pumping station. Using the variance analysis, the
315 degree of confidence for the achieved results by the regression equation was
316 determined, and the suitability of this equation at every point of the experimental
317 field.

318 The model which was elaborated in this study, was successfully validated in the
319 statistical analysis. It shows that the R-square statistic reaching 0.91, and a standard

320 error of estimate of 0.05. Thus, due to the lack of previous studies using multiple
321 linear regression, we compared the results with a previous study involving five data-
322 mining approaches (Kusiak et al., 2013).

323 This study had for objective to model the energy consumption in a comparable
324 case of a wastewater pumping station that has 3 pumps that transfer the wastewater
325 to a treatment plant. Although there are differences between the flow capacities and
326 the pressure with drinking water supply facilities but the approach remains the
327 same. The five data mining approaches are the multi-layer, perceptron, neural
328 network (MLP), the boosted-tree (regression) algorithm (BT), the random-forest
329 algorithm (RF), the support-vector machine (SVM), and the k-nearest neighbor
330 algorithm. These approaches had all provided more than 90% of accuracy which is
331 the case in the model of this study. The benefit of our method goes beyond the
332 control methods used in most of the optimization approaches which only provide a
333 method to operate the system in an efficient way but don't account for other factors
334 such as the aging of the pumps, factors that are crucial when upgrading the system.

335

336 **4. Conclusions**

337 A Linear multiple regression was conducted to assess and study the influence of
338 multiple parameters on the energy consumption ratio per cubic meter water,
339 involved in a water pumping station.

340 This unique approach has allowed evaluating the real response of the system
341 relying on data that is measured over a 4 years period. Modelling the ratio will be a
342 tool to take decisions on which pump should the work be done first. This method
343 combined with a cash flow analysis, can help to take decisions on establishing
344 priorities in case of renovations, to change the pumps 1 and 4 with more efficient
345 pumps. To validate this model, we performed the performance test by determining
346 the correlation R to show the link between the produced kWh/m³ ratio and the
347 following parameters such as active and reactive energies, the daily produced water
348 volume, the power factor (Cosφ), and the operating time of each pump. the

349 regression coefficients, thus validating the models. The final model describes
350 accurately the consumption per cubic meter produced with a R-square statistic
351 reaching 0.91.

352 After this study, we retain that the developed model can predict the energy
353 consumption ratio per cubic meter water, involved in a water pumping station.
354 Thus, the model would be useful when the next renovation will be undertaken by
355 the office which will conduct a replacement of the pumps in the year 2024, can
356 more accurately and reasonably evaluate the efficiency pumping, according to the
357 pumping unit model, motor power...

358 Besides that, the above findings demonstrate the potential of method for solving
359 real-time pump scheduling problems in large water distribution systems with many
360 pumps. However, this requires further work with other metaheuristic methods such
361 as Genetic Algorithms before relevant conclusion can be made.

362

363 **Data availability.** The source data used for the illustrations of the cases are
364 available upon request.

365 **Conflict of interest.** All authors declare no conflicts of interest in this paper.

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