



1 Evaluation of Thin Film Composite Forward Osmosis Membranes: 2 Effect of Polyamide Preparation Conditions

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7 **Abstract** The forward osmosis (FO) process has been considered for desalination as a competitor option to the traditional
8 reverse osmosis process. Interfacial polymerization (IP) reaction between two monomers (i.e., m-phenylene diamine (MPD)
9 and 1, 3, 5-benzenetricarbonyl chloride (TMC)) is typically used to prepare the selective polyamide layer that prevents salts
10 and allows water molecules to pass. In this research, we investigated the effect of preparation conditions (MPD contact time,
11 TMC reaction time, and addition of an amine salt) on the FO performance in terms of water flux and salt flux. The results
12 showed that increasing MPD contact time resulted in a significant increase in the water flux and salt flux. However,
13 increasing TMC reaction time caused a decline in both the water flux and the salt flux. The optimum condition that gave the
14 highest water flux was found to be as 5 min for MPD and 1 min for TMC. The addition of an amine salt of camphorsulfonic
15 acid-triethylamine (CSA-TEA) was able to make an apparent effect on the FO process by increasing water flux.
16

17 **Keywords:** Forward Osmosis; Thin-Film Composite; Polysulfone; Interfacial Polymerization; Polyamide

18

19 1. Introduction

20 Water Purification is the process of removing pollutants from raw water to produce water for human consumption (drinking
21 water) or other beneficial purposes (irrigation, livestock, and industrial use). Membrane processes are among the most
22 effective methods that can be used for water purification especially for desalination of water.

23 At this time, the most effective technique is the reverse osmosis (RO) process, where it can be used to desalinate seawater
24 and also for wastewater reuse (Kadhom et al., 2019; Kalash et al., 2020). RO can be defined as the process that relies on
25 external force, in which the applied hydraulic pressure is responsible for transporting water through the membrane (Peñate
26 and García-Rodríguez, 2012).

27 Forward osmosis (FO) is an osmotically driven membrane process that uses the osmotic pressure gradient to drive water
28 transport across a semi-permeable membrane while rejecting most solutes (Cath et al., 2006; McCutcheon et al., 2005). In
29 the FO process, water transports from a low osmotic pressure solution (i.e., feed solution) to a higher osmotic pressure
30 solution (i.e., draw solution). Besides, FO has been considered a high water recovery and low-cost purification option
31 compared to the pressure-driven membrane processes like reverse osmosis (Linares et al., 2017). One of the most critical
32 factors affecting the development of the FO process is preparing a suitable membrane for the process. The ideal membranes
33 for FO have to be able to provide high water permeability, high rejection of solutes, substantially reducing internal
34 concentration polarization (ICP), and has high chemical stability and mechanical strength (Ren and McCutcheon, 2014;
35 Zhao et al., 2012).

36 Thin-film composite (TFC) membranes have been studied widely for FO applications (Al-Furaiji et al., 2019; Chowdhury et
37 al., 2017; Ren and McCutcheon, 2017). TFC membranes consist of two layers: a selective layer that only allows water to
38 pass and rejects salt and a support layer that gives the membrane the required mechanical properties. Most of the FO studies
39 on TFC membranes have been focusing on developing the support layer, while fewer studies have been considering
40 improving the selective layer.



41 The preparation of the polyamide selective layer is conducted using interfacial polymerization (IP) reaction
42 (Mohammadifakhr et al., 2020). Typically, the IP reaction occurs between two reactive monomers: m-phenylene diamine
43 (MPD) in the aqueous phase with 1, 3, 5-benzenetricarbonyl chloride (TMC) in the organic phase (Raaijmakers and Benes,
44 2016). Previous studies have reported that controlling the IP reaction conditions could significantly affect the performance of
45 the formed polyamide layer (Kadhom and Deng, 2019a) however, most of these studies were dealing with reverse osmosis
46 membranes (Dong et al., 2015; Jin and Su, 2009; Zhao et al., 2013). In contrast, very few studies have investigated the effect
47 of interfacial polymerization reaction on the performance of the TFC FO membranes (Klaysom et al., 2013). Therefore,
48 studying the effect of the preparation conditions can help in preparing highly efficient FO membranes.

49 In this work, the effect of m-phenylenediamine (MPD) aqueous solution exposure time and trimesoyl chloride (TMC)
50 organic solution reaction time is studied. Besides, the effect of incorporating an amine salt to the MPD solution was reported.
51 This paper aims to study the conditions of the interfacial polymerization reaction on the efficiency of the TFC membranes in
52 the FO process. Scanning electron microscopy (SEM), atomic force microscopy (AFM), and contact angles measurements
53 were used to characterize the prepared membranes.

54 2. Materials and Methods

55 2.1. Materials

56 Polysulfone (PSU, MW= 22000) from Xian Lyphar Biotech, China, was used to fabricate membranes substrates. N,N
57 dimethylformamide (DMF, 99.8%) and 2,2,4-trimethylpentane (isooctane, 99%) were purchased from Fluka Chemie
58 AG, Buchs, Switzerland. M-phenylenediamine (MPD, >99%) and trimesoyl chloride (TMC, 98%) were ordered from Merck.
59 Triethylamine (TEA, ≥99%), and (1s)- 10-(+)camphorsulfonic acid (CSA, 99%), were purchased from Sigma Aldrich.
60 Sodium chloride (NaCl) was purchased from Thomas Baker, India. Deionized water (DI water) was used to prepare NaCl
61 and MPD aqueous solutions and for other purposes such as cleaning.

62 2.2. Preparation of PSU support layer

63 The phase inversion method was used to prepare PSU supporting sheets. The casting solution was prepared by dissolving 17
64 wt. % dry polysulfone pellets in DMF. The mixture was stirred and heated to 60°C for 6 h until a clear solution was formed,
65 which was then degassed for more than 24 h at room temperature before use. Afterward, the solution was cast using a home-
66 made casting knife by taking an aliquot from the clear solution by a pipette to spread on a clean glass plate to the desired
67 thickness. The glass plate with the solution was then immersed into a water bath at room temperature resulting in the
68 immediate formation of the PSU support sheet that was separated from the glass plate in a moment. Then, all of the sheets
69 were collected and stored in DI water for 24 h or more at 4°C before use.

70 2.3. Preparation of TFC membrane

71 TFC Forward osmosis membranes were fabricated on the top surface of the PSU sheet by interfacial polymerization reaction
72 between MPD aqueous solution and TMC organic solution. MPD aqueous solution was prepared by dissolving 2% MPD in
73 DI water while the TMC solution was made by dissolving 0.15% of TMC in isooctane. Firstly the MPD solution was poured
74 onto the PSU sheet at different contact times. Then, the TMC solution was poured onto the PSU sheet that is containing the
75 MPD active sites and the reaction time was also varied to study the effect of IP reaction time. At first, the MPD contact time
76 was varied from 2 to 5 min with keeping the contact time of the TMC at 1 min. Then, the best MPD contact time (i.e. 5
77 minutes) that gave the highest water flux was chosen and the TMC solution contact time was studied in the range of 1 to 4
78 minutes. In order to study the effect of adding CSA-TEA (2:1), they were added to the MPD solution with a weight percent



79 of 1%. The IP reaction was conducted at room temperature. Finally, the obtained TFC membranes were dried in the oven at
80 60°C for 10 min and then collected and stored in DI water for 24 h until testing.

81 **2.4. Membrane characterization**

82 Scanning Electron Microscope (Fesem Tescan Mira3 France) and Atomic Force Microscope (Angstrom advanced Inc.,
83 2008, U.S.A) were used to determine the morphology of the prepared membrane. The hydrophilicity of the membranes was
84 measured using contact angles (Theta Lite TL-101 Thailand).

85 **2.5. FO performance test**

86 The FO performance was tested in a bench-scale system, as shown in Figure 1. This system consists of two tanks: one of
87 them is used for the feed solution and the other contains the draw solution. DI water was used as a feed solution while 1 M
88 NaCl was used as a draw solution based on the standard methodology that was described by (Cath et al., 2013). These
89 solutions were pumped to the membrane cell using two pumps from Pure-water (model: 75GPD, volts: 24VDC, workflow:
90 28LPH). All experiments were conducted in FO mode (i.e., active layer faces the feed solution). The membrane was
91 installed in a custom-made cell with the chamber's dimensions of length 7.62 cm, width 2.54 cm and a depth of 0.3 cm.
92 Water flux J_w can be estimated using the following equation (Al-Furaiji et al., 2018):

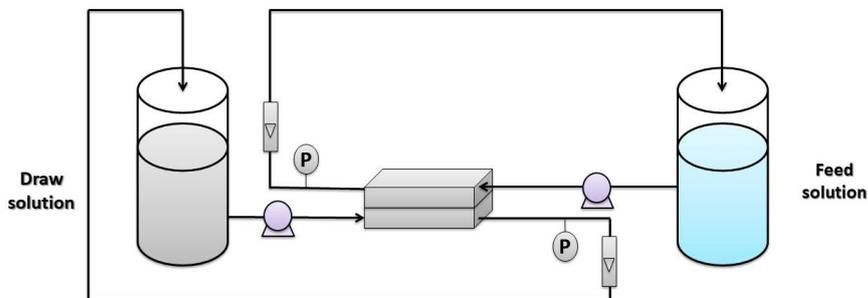
$$93 J_w = \frac{\Delta V}{At}$$

94 Where J_w is the water flux (LMH: $\text{Lm}^{-2} \text{h}^{-1}$), ΔV is the change in feed solution volume (L), A is the active area of the
95 membrane (m^2), and t is the experiment's time (h).

96 Salt flux through the membrane was estimated by monitoring the change in conductivity of the feed solution and using the
97 following equation (Al-Furaiji et al., 2020):

$$98 J_s = \frac{\Delta CV}{At}$$

99 Where J_s is the salt flux (GMH: $\text{gm}^{-2} \text{h}^{-1}$), ΔC is the change in the feed solution concentration (g/L), V is the volume of
100 feedwater flow (L), A is the active area of the membrane (m^2), and t is the experiment's time (h).



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Figure 1. Schematic diagram of the FO bench-scale test unit.

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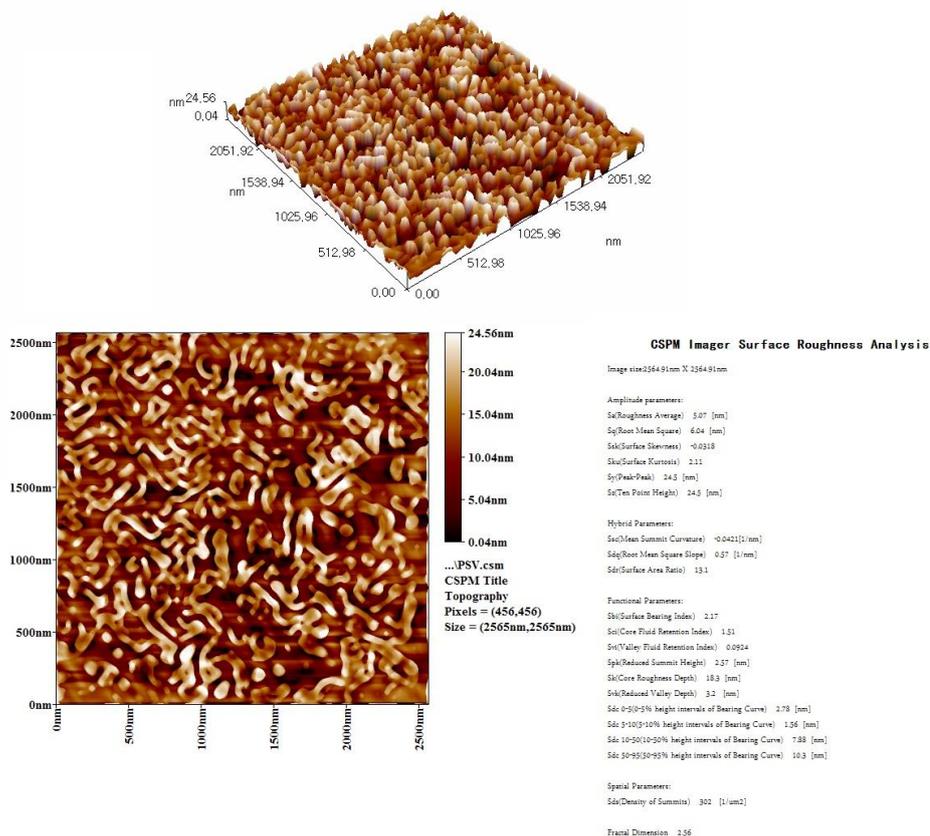
104 3. Results and discussion

105 3.1. Membrane characterization

106 Two dimensional (2D) and three dimensional (3D) AFM images of the top surface of the TFC membrane are presented in a
107 scan area of 2500 x 2500 nm, as shown in Figure 2. It can be clearly seen that the surface of the polyamide layer has a ridge-
108 and-valley structure with an average roughness of the FO membrane surface is 5.07 nm. The surface roughness of the
109 prepared membrane was quite similar to what has been reported for typical FO (Mi and Elimelech, 2008) and Nanofiltration
110 membranes (Li et al., 2017, 2020). The rougher surface could be more beneficial for membrane performance as it gives
111 higher areas for mass transfer especially when dealing with low fouling feed solution.

112 SEM images were used to investigate the surface morphology of the TFC membranes, as shown in Figure 3. It can be seen
113 that the polyamide selective membrane was successfully formed on the PSU support sheet. This was confirmed by the leaf-
114 like morphology which is a typical structure for polyamide TFC membranes (Kadhom and Deng, 2019b; Zhou et al., 2014).

115 Figure 4 shows the contact angle measurement of the PSU support membrane and the polyamide selective layer. The contact
116 angle of the PSU sheet was about 65°, while the thin polyamide layer had a contact angle of 33°. When the contact angle is
117 small, that means the membrane is hydrophilic, meaning that the water penetrates easily into the pores of the membrane, so
118 that gives a better osmotic water flux performance. Nevertheless, when the contact angle is large, it means that the film is
119 hydrophobic, so the internal surfaces of the pores get dry. That gives a membrane with lower water flux.

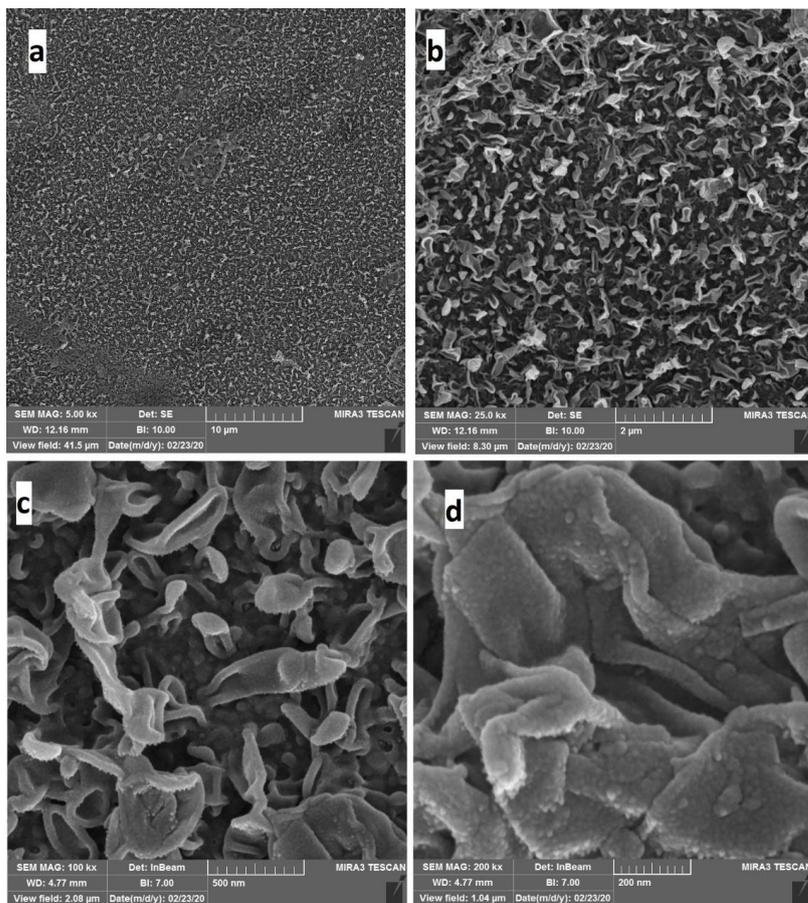


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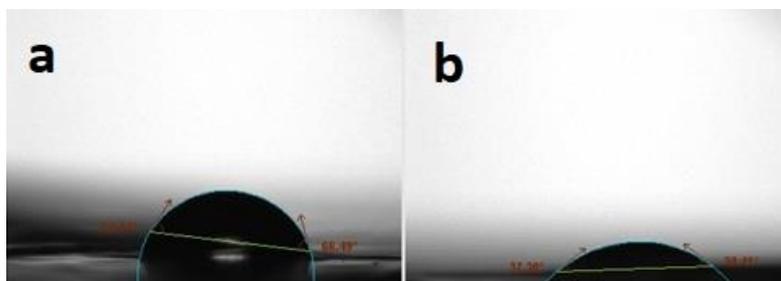
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Figure 2. AFM images of the TFC-FO membrane.



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124

Figure 3. SEM images of the TFC-FO membrane: a) 5000X, b) 25000X, c) 100000X, and d) 200000X.



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126
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Figure 4. The contact angle of a) PSU substrate membrane and b) polyamide thin layer.

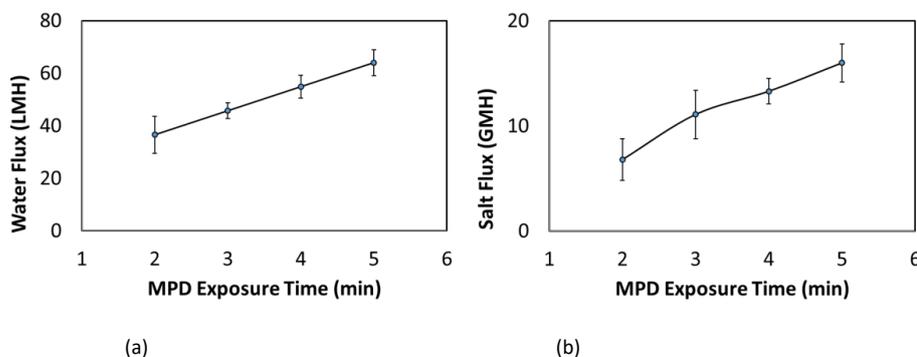
128 3.2. Effect of MPD exposure time

129 After the PSU support sheet has been prepared, the active layer is prepared by pouring the MPD solution onto the PSU layer
130 after fixing it well on a glass plate. The effect of MPD exposure time on the performance of the TFC-FO membrane was



131 studied by varying the contact time from 2 to 5 minutes while fixing the TMC reaction time at 1 minute, as shown in Figure
132 5.

133 The osmotic performance results revealed that water flux increases when the MPD exposure time increases. Also, increasing
134 the MPD contact time leads to increasing salt flux. In fact, higher MPD exposure time means more MPD molecules would
135 react with the support layer and accordingly increasing the IP reaction active sites. Besides, well-formed crosslinking would
136 be achieved at higher MPD exposure time, which gives better IP reaction conditions when reacts with the TMC later
137 (Kadhom and Deng, 2019a).



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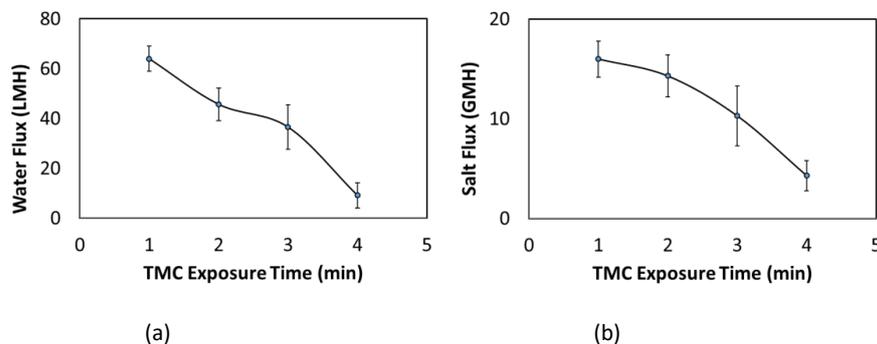
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140 **Figure 5. The effect of MPD contact time on membrane performance. (a) The water flux (LMH) changing with**
141 **different MPD exposure time (min.). (b) The salt flux (GMH) changing with different MPD exposure time (min.).**

142

3.3. Effect of TMC reaction time

143 In order to study the effect of IP reaction time, TMC contact time was varied from 1 to 4 min with fixing the MPD exposure
144 time at 5 min, as shown in Figure 6. TMC organic solution was poured on the PSU substrate that contains the MPD active
145 sites to conduct the IP reaction. It can be seen that the optimum condition that gave the highest water flux was recorded at a
146 reaction time of 1 min. Interestingly, it can also be noticed that water flux and salt flux decreased sharply with increasing the
147 TMC reaction time. This is mainly attributed to that increasing the TMC contact time leads to generating a thicker polyamide
148 layer and consequently higher mass transfer resistance to permeation of water (Zhou et al., 2014). Moreover, the extent of the
149 cross-linking is increased with increasing the IP reaction time and as a result, water flux and salt flux decreased (Wang et al.,
150 2017).



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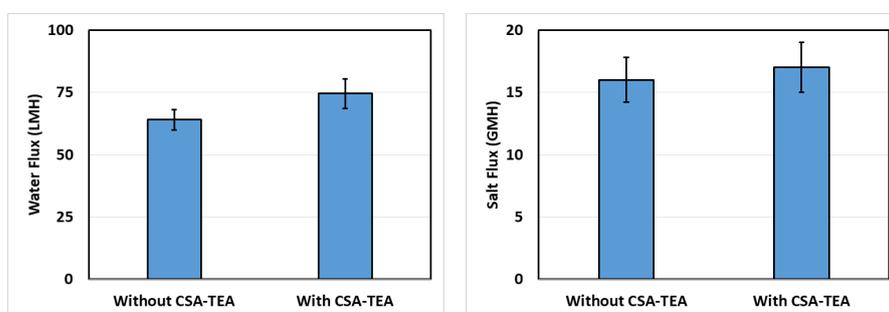
153 **Figure 6. The effect of TMC contact time on membrane performance. (a) The water flux (LMH) changing with**
154 **different TMC exposure time (min.). (b) The salt flux (GMH) changing with different TMC exposure time (min.).**

155



156 3.4. Effect of CSA-TEA salt

157 The effect of adding an amine salt (i.e., CSA-TEA) on the performance of the FO process was studied as shown in Figure 7.
158 It has been found that adding 1% of the CSA-TEA to the aqueous MPD solution exhibited a moderate increase in both water
159 flux and salt flux. Similar behavior was reported for reverse osmosis and Nanofiltration processes (Khorshidi et al., 2017). It
160 is known that polyamide formation during the IP reaction can result in the release of hydrogen chloride (Raaijmakers and
161 Benes, 2016). The formation of hydrogen chloride can affect the reactivity of the monomer reactant in the aqueous phase
162 (i.e., MPD). Therefore, the addition of a strong base such as TEA enhances the reactivity of the MPD and consumes the
163 produced acid (i.e. hydrogen chloride). Also, it has been reported that the TEA acts as a catalyst by accelerating the MPD–
164 TMC reaction and generating thinner and more crosslinked polyamide layer (Vatanpour et al., 2017; Wang et al., 2017).



165

166 (a)

(b)

167 **Figure 7. The effect of adding CSA-TEA to the MPD-aqueous solution on a) water flux and b) salt flux.**

168

169 4. Conclusion

170 In this work, TFC forward osmosis membranes were prepared on PSU substrate (17wt %) as a support layer via IP reaction
171 between MPD and TMC to form a polyamide selective layer. The effect of MPD and TMC reaction times was investigated.
172 The best results were found to be at 5 min for MPD and 1 min for TMC reaction times. These results gave the best
173 performance of FO membranes in terms of water flux and salt rejection. Increasing MPD exposure time leads to increasing
174 the active sites on the PSU layer. By changing the TMC reaction time, it is possible to control how dense the polyamide
175 layer and, consequently, the amount of water and salt that passes through the membrane. Also, the effect of adding an amine
176 salt (CSA-TEA) on the performance of FO membranes was demonstrated. The result showed that moderate improvement in
177 water flux was achieved. Finally, this study can be considered as a useful guide for researchers and workers in the field of
178 preparing TFC forward osmosis. Future research can focus on investigating other additives to the MPD and TMC solutions.
179 Also, studying the effect of changing MPD and TMC concentrations in preparing TFC-FO is highly recommended for future
180 works.

181 Declaration of competing interest

182 The authors declare that they have no known competing financial interests or personal relationships that could have appeared
183 to influence the work reported in this paper.

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