

1 Evaluation of Thin Film Composite Forward Osmosis Membranes: 2 Effect of Polyamide Preparation Conditions

3 Aya Mohammed Kadhom ¹, Mustafa Hussein Al-Furaiji ², Zaidun Naji Abudi ¹

4 ¹ Environmental Engineering Department, College of Engineering, Mustansiriyah University, Iraq

5 ² Environment and Water Directorate, Ministry of Science and Technology, Baghdad, Iraq

6 *Correspondence to:* Mustafa Al-Furaiji (alfuraiji79@gmail.com)

7 **Abstract** The forward osmosis (FO) process has been considered for desalination as a competitor option to the traditional
8 reverse osmosis process. Interfacial polymerization (IP) reaction between two monomers (i.e., m-phenylene diamine (MPD)
9 and 1, 3, 5-benzenetricarbonyl chloride (TMC)) is typically used to prepare the selective polyamide layer that prevents salts
10 and allows water molecules to pass. In this research, we investigated the effect of preparation conditions (MPD contact time,
11 TMC reaction time, and addition of an amine salt) on the FO performance in terms of water flux and salt flux. The results
12 showed that increasing MPD contact time resulted in a significant increase in the water flux and salt flux. However,
13 increasing TMC reaction time caused a decline in both the water flux and the salt flux. The optimum condition that gave the
14 highest water flux (64 L.m⁻².h⁻¹) was found to be as 5 min for MPD and 1 min for TMC. The addition of an amine salt of
15 camphorsulfonic acid-triethylamine (CSA-TEA) was able to make an apparent effect on the FO process by increasing water
16 flux (74.5 L.m⁻².h⁻¹).
17

18 **Keywords:** Forward Osmosis; Thin-Film Composite; Polysulfone; Interfacial Polymerization; Polyamide
19

20 1. Introduction

21 Water Purification is the process of removing pollutants from raw water to produce water for human consumption (drinking
22 water) or other beneficial purposes (irrigation, livestock, and industrial use) (Maddodi et al., 2020). Membrane processes are
23 among the most effective methods that can be used for water purification especially for desalination of water.

24 At this time, the most effective technique is the reverse osmosis (RO) process, where it can be used to desalinate seawater
25 and also for wastewater reuse (Kadhom et al., 2019; Kalash et al., 2020). RO can be defined as the process that relies on
26 external force, in which the applied hydraulic pressure is responsible for transporting water through the membrane (Peñate
27 and García-Rodríguez, 2012).

28 Forward osmosis (FO) is an osmotically driven membrane process that uses the osmotic pressure gradient to drive water
29 transport across a semi-permeable membrane while rejecting most solutes (Cath et al., 2006; McCutcheon et al., 2005). In
30 the FO process, water transports from a low osmotic pressure solution (i.e., feed solution) to a higher osmotic pressure
31 solution (i.e., draw solution). Besides, FO has been considered a high water recovery and low-cost purification option
32 compared to the pressure-driven membrane processes like reverse osmosis (Linares et al., 2017). One of the most critical
33 factors affecting the development of the FO process is preparing a suitable membrane for the process. The ideal membranes
34 for FO have to be able to provide high water permeability, high rejection of solutes, substantially reducing internal
35 concentration polarization (ICP), and has high chemical stability and mechanical strength (Ren and McCutcheon, 2014;
36 Zhao et al., 2012).

37 Thin-film composite (TFC) membranes have been studied widely for FO applications (Al-Furaiji et al., 2019; Chowdhury et
38 al., 2017; Ren and McCutcheon, 2017). TFC membranes consist of two layers: a selective layer that only allows water to
39 pass and rejects salt and a support layer that gives the membrane the required mechanical properties. Most of the FO studies

40 on TFC membranes have been focusing on developing the support layer, while fewer studies have been considering
41 improving the selective layer.

42 The preparation of the polyamide selective layer is conducted using interfacial polymerization (IP) reaction
43 (Mohammadifakhr et al., 2020). Typically, the IP reaction occurs between two reactive monomers: m-phenylene diamine
44 (MPD) in the aqueous phase with 1, 3, 5-benzenetricarbonyl chloride (TMC) in the organic phase (Raaijmakers and Benes,
45 2016). Previous studies have reported that controlling the IP reaction conditions could significantly affect the performance of
46 the formed polyamide layer (Kadhom and Deng, 2019a) however, most of these studies were dealing with reverse osmosis
47 membranes (Dong et al., 2015; Jin and Su, 2009; Zhao et al., 2013). In contrast, very few studies have investigated the effect
48 of interfacial polymerization reaction on the performance of the TFC FO membranes (Klaysom et al., 2013). Therefore,
49 studying the effect of the preparation conditions can help in preparing highly efficient FO membranes.

50 In this work, the effect of m-phenylenediamine (MPD) aqueous solution exposure time and trimesoyl chloride (TMC)
51 organic solution reaction time is studied. Besides, the effect of incorporating an amine salt to the MPD solution was reported.
52 This paper aims to study the conditions of the interfacial polymerization reaction on the efficiency of the TFC membranes in
53 the FO process. Scanning electron microscopy (SEM), atomic force microscopy (AFM), and contact angles measurements
54 were used to characterize the prepared membranes.

55 **2. Materials and Methods**

56 **2.1. Materials**

57 Polysulfone (PSU, MW= 22000) from Xian Lyphar Biotech, China, was used to fabricate membranes substrates. N,N
58 dimethylformamide (DMF, 99.8%) and 2,2,4-trimethylpentane (isooctane, 99%) were purchased from Fluka Chemie
59 AG, Buchs, Switzerland. M-phenylenediamine (MPD, >99%) and trimesoyl chloride (TMC, 98%) were ordered from Merck.
60 Triethylamine (TEA, $\geq 99\%$), and (1s)- 10-(+)camphorsulfonic acid (CSA, 99%), were purchased from Sigma Aldrich.
61 Sodium chloride (NaCl) was purchased from Thomas Baker, India. Deionized water (DI water) was used to prepare NaCl
62 and MPD aqueous solutions and for other purposes such as cleaning.

63 **2.2. Preparation of PSU support layer**

64 The phase inversion method was used to prepare PSU supporting sheets. The casting solution was prepared by dissolving 17
65 wt. % dry polysulfone pellets in DMF. The mixture was stirred and heated to 60°C for 6 h until a clear solution was formed,
66 which was then degassed for more than 24 h at room temperature before use. Afterward, the solution was cast using a home-
67 made casting knife by taking an aliquot from the clear solution by a pipette to spread on a clean glass plate to the desired
68 thickness. The glass plate with the solution was then immersed into a water bath at room temperature resulting in the
69 immediate formation of the PSU support sheet that was separated from the glass plate in a moment. Then, all of the sheets
70 were collected and stored in DI water for 24 h or more at 4°C before use.

71 **2.3. Preparation of TFC membrane**

72 TFC Forward osmosis membranes were fabricated on the top surface of the PSU sheet by interfacial polymerization reaction
73 between MPD aqueous solution and TMC organic solution. MPD aqueous solution was prepared by dissolving 2% MPD in
74 DI water while the TMC solution was made by dissolving 0.15% of TMC in isooctane. Firstly the MPD solution was poured
75 onto the PSU sheet at different contact times. Then, the TMC solution was poured onto the PSU sheet that is containing the
76 MPD active sites and the reaction time was also varied to study the effect of IP reaction time. At first, the MPD contact time
77 was varied from 2 to 5 min with keeping the contact time of the TMC at 1 min. Then, the best MPD contact time (i.e. 5
78 minutes) that gave the highest water flux was chosen and the TMC solution contact time was studied in the range of 1 to 4

79 minutes. In order to study the effect of adding CSA-TEA at a weight ratio of 2:1, they were added to the MPD solution with
80 a weight percent of 1%. The IP reaction was conducted at room temperature. Finally, the obtained TFC membranes were
81 dried in the oven at 60°C for 10 min and then collected and stored in DI water for 24 h until testing.

82 2.4. Membrane characterization

83 Scanning Electron Microscope (Fesem Tescan Mira3 France) and Atomic Force Microscope (Angstrom advanced Inc.,
84 2008, U.S.A) were used to determine the morphology of the prepared membrane. The hydrophilicity of the membranes was
85 measured using contact angles (Theta Lite TL-101 Thailand).

86 2.5. FO performance test

87 The FO performance was tested in a bench-scale system, as shown in Figure 1. This system consists of two tanks: one of
88 them is used for the feed solution and the other contains the draw solution. DI water was used as a feed solution while 1 M
89 NaCl was used as a draw solution based on the standard methodology that was described by (Cath et al., 2013). These
90 solutions were pumped to the membrane cell using two pumps from Pure-water (model: 75GPD, volts: 24VDC, workflow:
91 28LPH). All experiments were conducted in FO mode (i.e., active layer faces the feed solution). The membrane was
92 installed in a custom-made cell with the chamber's dimensions of length 7.62 cm, width 2.54 cm and a depth of 0.3 cm.
93 Water flux J_w can be estimated using the following equation (Al-Furaiji et al., 2018):

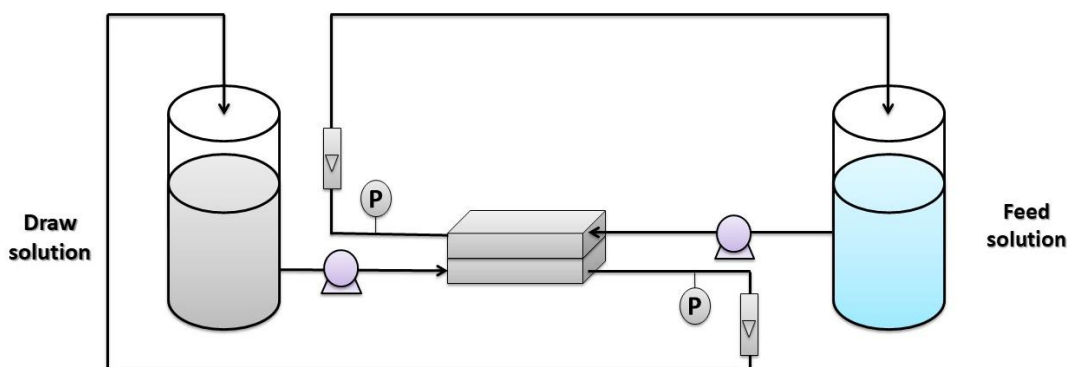
$$94 J_w = \frac{\Delta V}{At}$$

95 Where J_w is the water flux (LMH: $\text{Lm}^{-2} \text{h}^{-1}$), ΔV is the change in feed solution volume (L), A is the active area of the
96 membrane (m^2), and t is the experiment's time (h).

97 Salt flux through the membrane was estimated by monitoring the change in conductivity of the feed solution and using the
98 following equation (Al-Furaiji et al., 2020):

$$99 J_s = \frac{\Delta CV}{At}$$

100 Where J_s is the salt flux (GMH: $\text{gm}^{-2} \text{h}^{-1}$), ΔC is the change in the feed solution concentration (g/L), V is the volume of
101 feedwater flow (L), A is the active area of the membrane (m^2), and t is the experiment's time (h).



102

103

Figure 1. Schematic diagram of the FO bench-scale test unit. (Al-Furaiji et al., 2018)

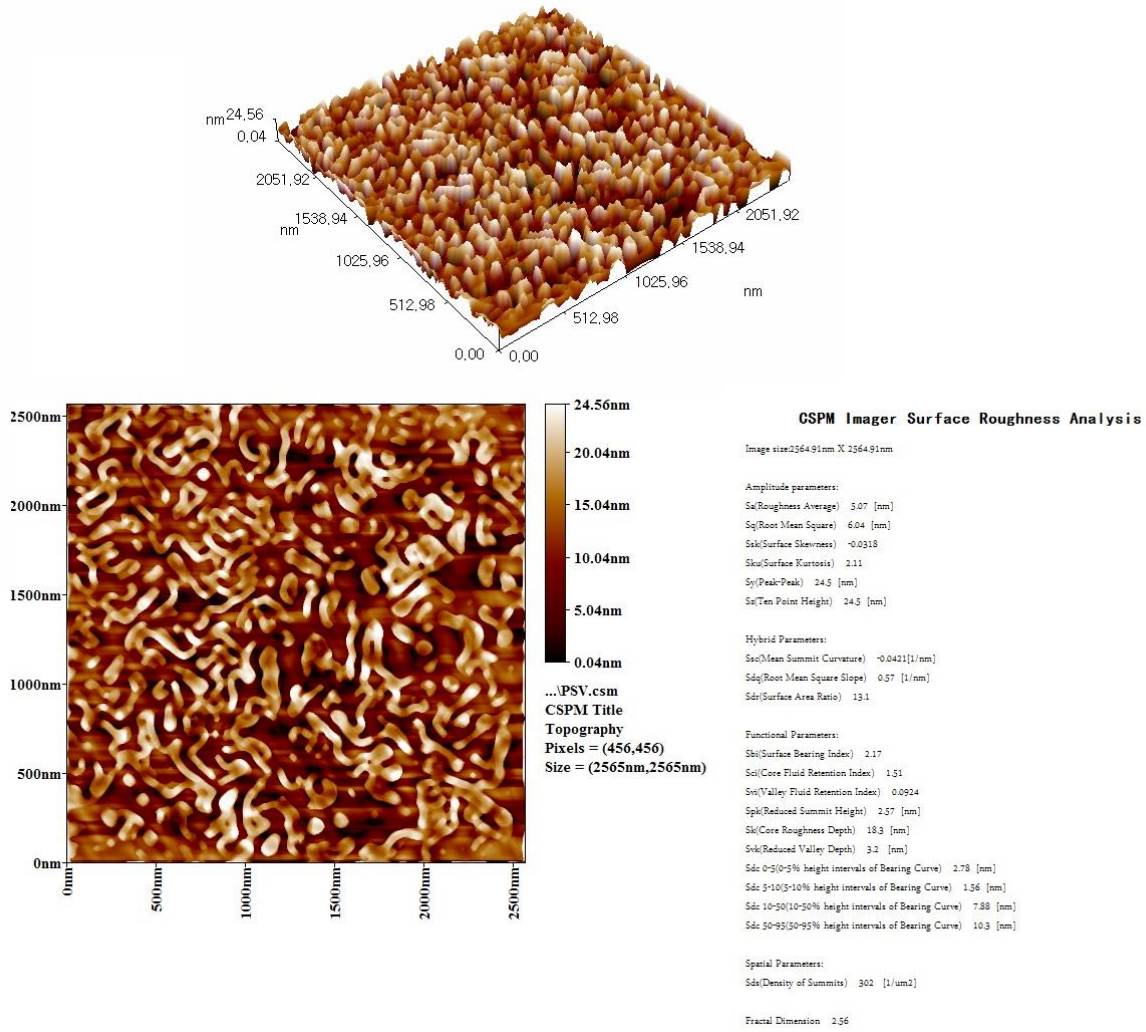
105 3. Results and discussion

106 3.1. Membrane characterization

107 Two dimensional (2D) and three dimensional (3D) AFM images of the top surface of the TFC membrane are presented in a
108 scan area of 2500 x 2500 nm, as shown in Figure 2. It can be clearly seen that the surface of the polyamide layer has a ridge-
109 and-valley structure with an average roughness of the FO membrane surface is 5.07 nm. The surface roughness of the
110 prepared membrane was quite similar to what has been reported for typical FO (Mi and Elimelech, 2008) and Nanofiltration
111 membranes (Li et al., 2017, 2020). The rougher surface could be more beneficial for membrane performance as it gives
112 higher areas for mass transfer especially when dealing with low fouling feed solution.

113 SEM images were used to investigate the surface morphology of the TFC membranes, as shown in Figure 3. It can be seen
114 that the polyamide selective membrane was successfully formed on the PSU support sheet. This was confirmed by the leaf-
115 like morphology which is a typical structure for polyamide TFC membranes (Kadhom and Deng, 2019b; Zhou et al., 2014).

116 Figure. 4 shows the contact angle measurement of the PSU support membrane and the polyamide selective layer. The contact
117 angle of the PSU sheet was about 65°, while the thin polyamide layer had a contact angle of 33°. When the contact angle is
118 small, that means the membrane is hydrophilic, meaning that the water penetrates easily into the pores of the membrane, so
119 that gives a better osmotic water flux performance. Nevertheless, when the contact angle is large, it means that the film is
120 hydrophobic, so the internal surfaces of the pores get dry. That gives a membrane with lower water flux.



121

122

123

Figure 2. AFM images of the TFC-FO membrane.

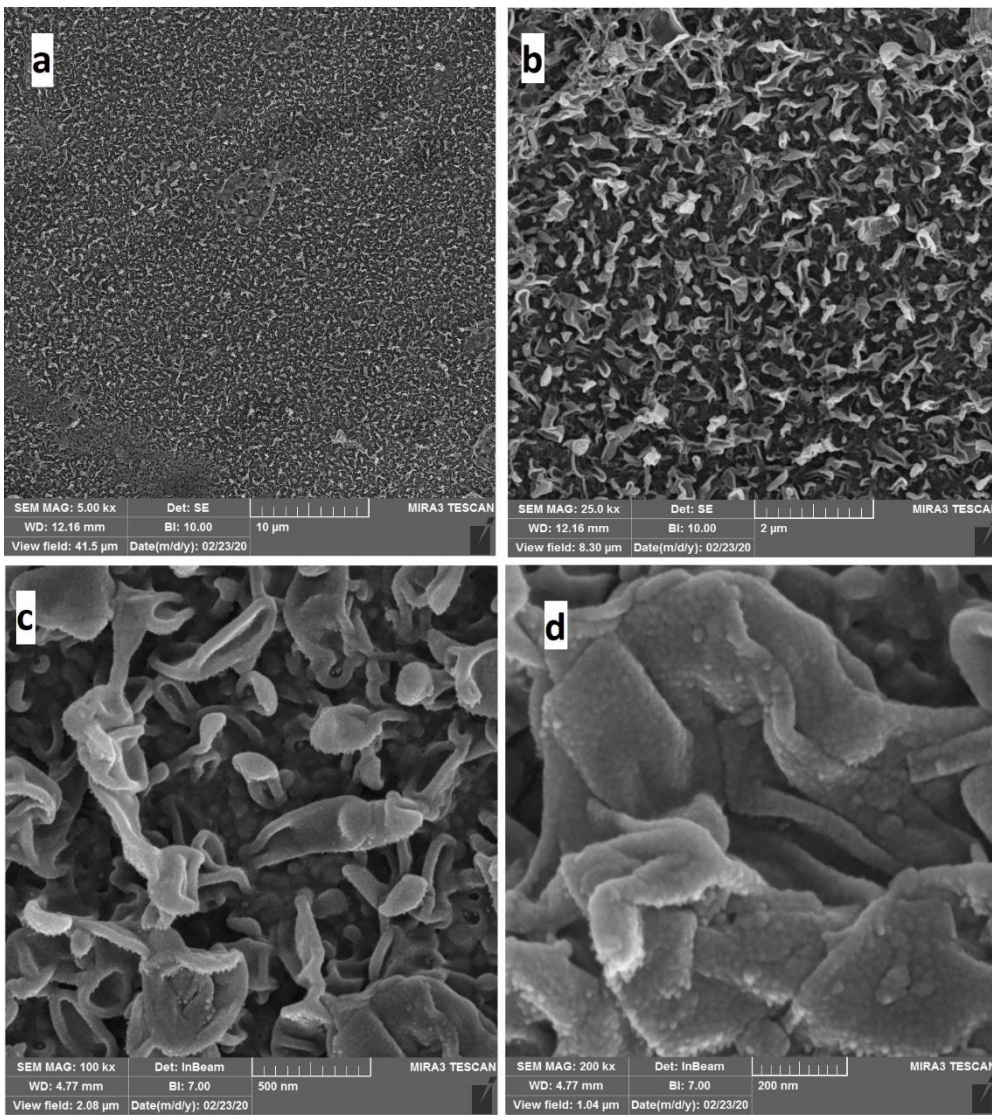


Figure 3. SEM images of the TFC-FO membrane: a) 5000X, b) 25000X, c) 100000X, and d) 200000X.

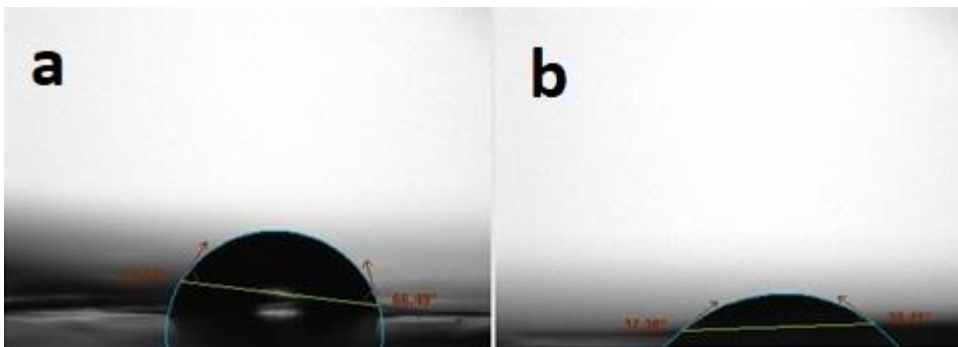
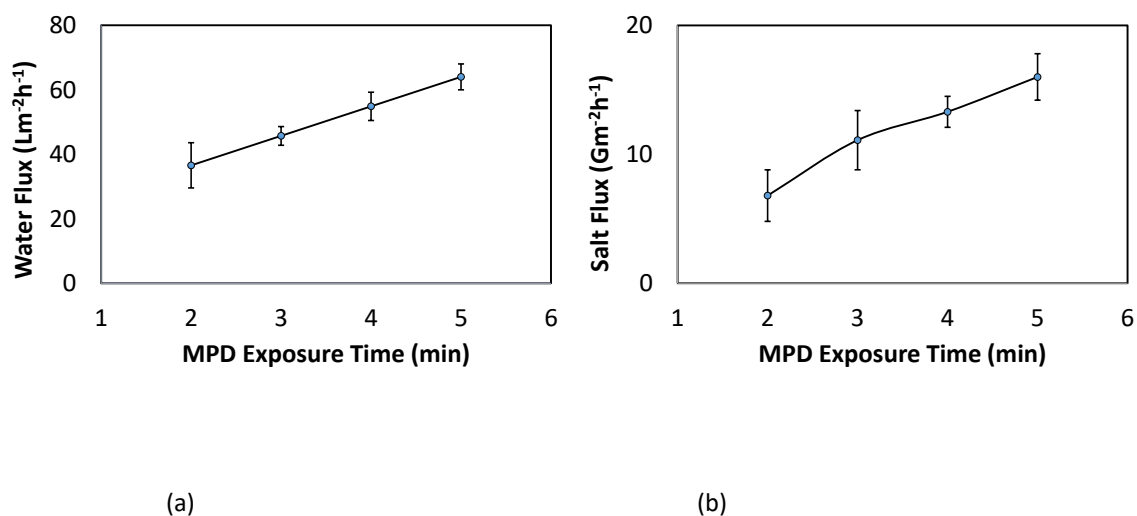


Figure 4. The contact angle of a) PSU substrate membrane and b) polyamide thin layer.

3.2. Effect of MPD exposure time

After the PSU support sheet has been prepared, the active layer is prepared by pouring the MPD solution onto the PSU layer after fixing it well on a glass plate. The effect of MPD exposure time on the performance of the TFC-FO membrane was studied by varying the contact time from 2 to 5 minutes while fixing the TMC reaction time at 1 minute, as shown in Figure 5.

134 The osmotic performance results revealed that water flux increases when the MPD exposure time increases. Also, increasing
 135 the MPD contact time leads to increasing salt flux. In fact, higher MPD exposure time means more MPD molecules would
 136 react with the support layer and accordingly increasing the IP reaction active sites. Besides, well-formed crosslinking would
 137 be achieved at higher MPD exposure time, which gives better IP reaction conditions when reacts with the TMC later
 138 (Kadhom and Deng, 2019a).



139

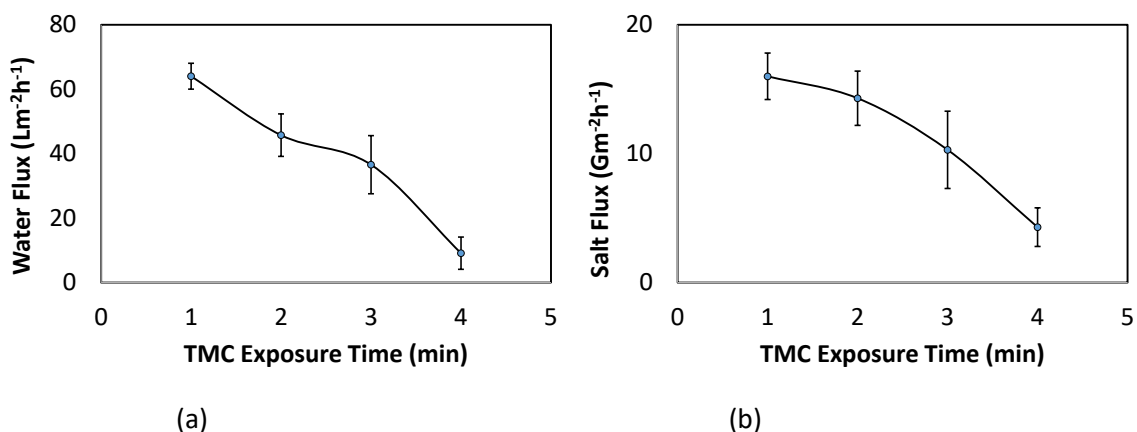
140

141

142 **Figure 5. The effect of MPD contact time on membrane performance. Feed solution: DI water and draw solution: 1M**
 143 **NaCl. (a) The water flux changing with different MPD exposure time (min.). (b) The salt flux changing with different**
 144 **MPD exposure time (min.).**

145 **3.3. Effect of TMC reaction time**

146 In order to study the effect of IP reaction time, TMC contact time was varied from 1 to 4 min with fixing the MPD exposure
 147 time at 5 min, as shown in Figure 6. TMC organic solution was poured on the PSU substrate that contains the MPD active
 148 sites to conduct the IP reaction. It can be seen that the optimum condition that gave the highest water flux was recorded at a
 149 reaction time of 1 min. Interestingly, it can also be noticed that water flux and salt flux decreased sharply with increasing the
 150 TMC reaction time. This is mainly attributed to that increasing the TMC contact time leads to generating a thicker polyamide
 151 layer and consequently higher mass transfer resistance to permeation of water(Zhou et al., 2014). Moreover, the extent of the
 152 cross-linking is increased with increasing the IP reaction time and as a result, water flux and salt flux decreased (Wang et al.,
 153 2017).



154

155

156 **Figure 6. The effect of TMC contact time on membrane performance. Feed solution: DI water and draw solution: 1M**
 157 **NaCl. (a) The water flux changing with different TMC exposure time (min.). (b) The salt flux changing with different**
 158 **TMC exposure time (min.).**

159

3.4. Effect of CSA-TEA salt

The effect of adding an amine salt (i.e., CSA-TEA) on the performance of the FO process was studied as shown in Figure 7. It has been found that adding 1% of the CSA-TEA to the aqueous MPD solution exhibited a moderate increase in both water flux and salt flux. Similar behavior was reported for reverse osmosis and Nanofiltration processes (Khorshidi et al., 2017). It is known that polyamide formation during the IP reaction can result in the release of hydrogen chloride (Raaijmakers and Benes, 2016). The formation of hydrogen chloride can affect the reactivity of the monomer reactant in the aqueous phase (i.e., MPD). Therefore, the addition of a strong base such as TEA enhances the reactivity of the MPD and consumes the produced acid (i.e. hydrogen chloride). Also, it has been reported that the TEA acts as a catalyst by accelerating the MPD–TMC reaction and generating thinner and more crosslinked polyamide layer (Vatanpour et al., 2017; Wang et al., 2017).

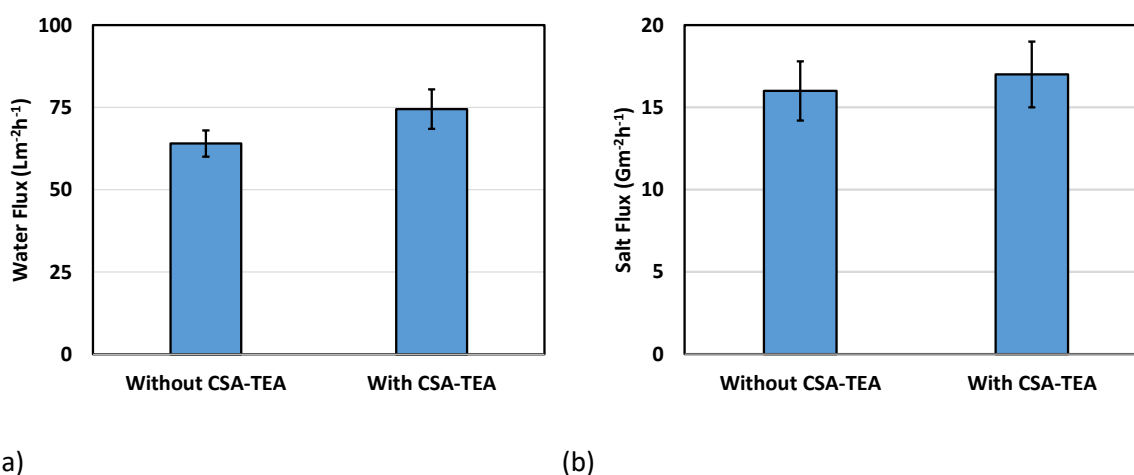


Figure 7. The effect of adding CSA-TEA to the MPD-aqueous solution on a) water flux and b) salt flux. Feed solution: DI water and draw solution: 1M NaCl.

A comparison of the TFC-PSU membrane with some of the previously reported TFC membranes can be found in Table 1. It can be seen that TFC-PSU membrane exhibited the highest water flux compared to the reported membranes. However, the reverse salt flux value lies within the range of the previously reported salt flux of the TFC membranes. If we look closely to the results of our previous work and compare it to the current work, it can be distinguished that the water flux of the current work is about twice that of the previous work, while the salt flux is a bit higher. There are two main differences between the previous work and the current work:

1. In the previous work, we used PAN polymer as a support for the TFC FO membrane, while in this work, we used PSU polymer.
2. In the previous work, the support layer was prepared using the electrospinning method while in this work phase inversion method was used.

The polyamide layer was perfectly formed and well distributed on the PSU support layer compared to the PAN nanofibers based membrane. This is most likely due to the smaller pore size and the hydrophobic nature of the PSU substrate. Although, electrospinning method produces a highly porous membrane, but phase inversion makes a more robust membrane that can perform better in FO testing.

Table 1. Comparison of the performance of some TFC membranes from previous studies.

| Membrane | Feed solution | Draw solution | Water flux (L/m ² h) | Salt flux (G/m ² h) | Reference |
|----------|---------------|---------------|------------------------------------|-----------------------------------|----------------------------|
| TFC-PSU | DI water | 1 M NaCl | 36.58 | 6.8 | This work. |
| HTI-TFC | DI water | 1 M NaCl | 15 | 4.5 | (Ren and McCutcheon, 2014) |
| TFC-PAN | DI water | 1 M NaCl | 16 | 4 | (Al-Furaiji et al., 2020) |

| | | | | | |
|---------------------------|----------|----------|------|------|---------------------|
| Aquaporin TFC | DI water | 1 M NaCl | 9 | 4 | (Xia et al., 2017) |
| TFC-M2 (CAB substrate) | DI water | 1 M NaCl | 16.8 | 5.88 | (Ma et al., 2020) |
| TFC-CTA (HTI, commercial) | DI water | 1 M NaCl | 12.0 | 8.04 | (Kwon et al., 2017) |
| CAB | DI water | 1 M NaCl | 9.0 | 3.78 | (Ong et al., 2012) |
| PVDF nanofiber-PA | DI water | 1 M NaCl | 11.6 | 3.48 | (Tian et al., 2013) |
| PSU /Silica-PA | DI water | 1M NaCl | 31 | 7.44 | (Liu and Ng, 2015) |
| Oasys TFC | DI water | 1M NaCl | 30 | 50 | (Cath et al., 2013) |

4. Conclusion

In this work, TFC forward osmosis membranes were prepared on PSU substrate (17wt %) as a support layer via IP reaction between MPD and TMC to form a polyamide selective layer. The effect of MPD and TMC reaction times was investigated. The best results were found to be at 5 min for MPD and 1 min for TMC reaction times. These results gave the best performance of FO membranes in terms of water flux and salt rejection. Increasing MPD exposure time leads to increasing the active sites on the PSU layer. By changing the TMC reaction time, it is possible to control how dense the polyamide layer and, consequently, the amount of water and salt that passes through the membrane. Also, the effect of adding an amine salt (CSA-TEA) on the performance of FO membranes was demonstrated. The result showed that moderate improvement in water flux was achieved. Finally, this study can be considered as a useful guide for researchers and workers in the field of preparing TFC forward osmosis. Future research can focus on investigating other additives to the MPD and TMC solutions. Also, studying the effect of changing MPD and TMC concentrations in preparing TFC-FO is highly recommended for future works.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgements

The author would like to thank Mustansiriyah University, Baghdad, Iraq, and the Ministry of Science and Technology in Iraq for their support in the present work.

5. References

- Al-Furaiji, M., Benes, N., Nijmeijer, A. and McCutcheon, J. R.: Use of a Forward Osmosis–Membrane Distillation Integrated Process in the Treatment of High-Salinity Oily Wastewater, *Ind. Eng. Chem. Res.*, 58(2), 956–962, doi:10.1021/acs.iecr.8b04875, 2019.
- Al-Furaiji, M., Kadhom, M., Kalash, K., Waisi, B. and Albayati, N.: Preparation of thin-film composite membranes supported with electrospun nanofibers for desalination by forward osmosis, *Drink. Water Eng. Sci.*, 13(2), 51–57, doi:10.5194/dwes-13-51-2020, 2020.
- Al-Furaiji, M. H. O., Arena, J. T., Chowdhury, M., Benes, N., Nijmeijer, A. and McCutcheon, J. R.: Use of forward osmosis in treatment of hyper-saline water, *Desalin. Water Treat.*, 133, 1–9, doi:10.5004/dwt.2018.22851, 2018.
- Cath, T. Y., Childress, A. E. and Elimelech, M.: *Forward osmosis: Principles, applications, and recent developments*, J.

- 217 Memb. Sci., 281(1–2), 70–87, doi:10.1016/j.memsci.2006.05.048, 2006.
- 218 Cath, T. Y., Elimelech, M., McCutcheon, J. R., McGinnis, R. L., Achilli, A., Anastasio, D., Brady, A. R., Childress, A. E.,
219 Farr, I. V., Hancock, N. T., Lampi, J., Nghiem, L. D., Xie, M. and Yip, N. Y.: Standard Methodology for Evaluating
220 Membrane Performance in Osmotically Driven Membrane Processes, *Desalination*, 312, 31–38,
221 doi:10.1016/j.desal.2012.07.005, 2013.
- 222 Chowdhury, M. R., Huang, L. and McCutcheon, J. R.: Thin Film Composite Membranes for Forward Osmosis Supported by
223 Commercial Nanofiber Nonwovens, *Ind. Eng. Chem. Res.*, 56(4), 1057–1063, doi:10.1021/acs.iecr.6b04256, 2017.
- 224 Dong, H., Zhao, L., Zhang, L., Chen, H., Gao, C. and Winston Ho, W. S.: High-flux reverse osmosis membranes
225 incorporated with NaY zeolite nanoparticles for brackish water desalination, *J. Memb. Sci.*, 476, 373–383,
226 doi:10.1016/j.memsci.2014.11.054, 2015.
- 227 Jin, Y. and Su, Z.: Effects of polymerization conditions on hydrophilic groups in aromatic polyamide thin films, *J. Memb.*
228 *Sci.*, 330(1–2), 175–179, doi:10.1016/j.memsci.2008.12.055, 2009.
- 229 Kadhom, M. and Deng, B.: Synthesis of high-performance thin film composite (TFC) membranes by controlling the
230 preparation conditions: Technical notes, *J. Water Process Eng.*, 30, 100542, doi:10.1016/j.jwpe.2017.12.011, 2019a.
- 231 Kadhom, M. and Deng, B.: Thin film nanocomposite membranes filled with bentonite nanoparticles for brackish water
232 desalination: A novel water uptake concept, *Microporous Mesoporous Mater.*, 279, 82–91,
233 doi:10.1016/j.micromeso.2018.12.020, 2019b.
- 234 Kadhom, M., Albayati, N., Salih, S., Al-Furaiji, M., Bayati, M. and Deng, B.: Role of Cellulose Micro and Nano Crystals in
235 Thin Film and Support Layer of Nanocomposite Membranes for Brackish Water Desalination, *Membranes (Basel)*, 9(8),
236 101, doi:10.3390/membranes9080101, 2019.
- 237 Kalash, K., Kadhom, M. and Al-Furaiji, M.: Thin film nanocomposite membranes filled with MCM-41 and SBA-15
238 nanoparticles for brackish water desalination via reverse osmosis, *Environ. Technol. Innov.*, 20, 101101,
239 doi:10.1016/j.eti.2020.101101, 2020.
- 240 Khorshidi, B., Thundat, T., Pernitsky, D. and Sadrzadeh, M.: permeation properties of thin film composite polyamide
241 membrane, *J. Memb. Sci.*, 535(December 2016), 248–257, doi:10.1016/j.memsci.2017.04.052, 2017.
- 242 Klaysom, C., Hermans, S., Gahlaut, A., Van Craenenbroeck, S. and Vankelecom, I. F. J.: Polyamide/Polyacrylonitrile
243 (PA/PAN) thin film composite osmosis membranes: Film optimization, characterization and performance evaluation, *J.*
244 *Memb. Sci.*, 445, 25–33, doi:10.1016/j.memsci.2013.05.037, 2013.
- 245 Kwon, S. J., Park, S. H., Park, M. S., Lee, J. S. and Lee, J. H.: Highly permeable and mechanically durable forward osmosis
246 membranes prepared using polyethylene lithium ion battery separators, *J. Memb. Sci.*, 544(March), 213–220,
247 doi:10.1016/j.memsci.2017.09.022, 2017.
- 248 Li, H., Shi, W., Du, Q., Zhou, R., Zhang, H. and Qin, X.: Improved separation and antifouling properties of thin-film
249 composite nanofiltration membrane by the incorporation of cGO, *Appl. Surf. Sci.*, 407, 260–275,
250 doi:10.1016/j.apsusc.2017.02.204, 2017.
- 251 Li, H., Shi, W., Zhang, H., Zhou, R. and Qin, X.: Preparation of internally pressurized polyamide thin-film composite hollow
252 fiber nanofiltration membrane with high ions selectivity by a facile coating method, *Prog. Org. Coatings*, 139(November),
253 105456, doi:10.1016/j.porgcoat.2019.105456, 2020.
- 254 Linares, R. V., Li, Z., Elimelech, M., Amy, G. and Vrouwenvelder, H.: Recent Developments in Forward Osmosis
255 Processes, *Water Intell. Online*, 16, 9781780408125, doi:10.2166/9781780408125, 2017.
- 256 Liu, X. and Ng, H. Y.: Fabrication of layered silica-polysulfone mixed matrix substrate membrane for enhancing
257 performance of thin-film composite forward osmosis membrane, *J. Memb. Sci.*, 481, 148–163,
258 doi:10.1016/j.memsci.2015.02.012, 2015.
- 259 Ma, J., Xiao, T., Long, N. and Yang, X.: The role of polyvinyl butyral additive in forming desirable pore structure for thin
260 film composite forward osmosis membrane, *Sep. Purif. Technol.*, 242(January), 116798, doi:10.1016/j.seppur.2020.116798,
261 2020.
- 262 Maddodi, S. A., Alalwan, H. A., Alminshid, A. H. and Abbas, M. N.: Isotherm and computational fluid dynamics analysis of
263 nickel ion adsorption from aqueous solution using activated carbon, *South African J. Chem. Eng.*, 32, 5–12,
264 doi:10.1016/j.sajce.2020.01.002, 2020.
- 265 McCutcheon, J. R., McGinnis, R. L. and Elimelech, M.: A novel ammonia-carbon dioxide forward (direct) osmosis
266 desalination process, *Desalination*, 174(1), 1–11, doi:10.1016/j.desal.2004.11.002, 2005.
- 267 Mi, B. and Elimelech, M.: Chemical and physical aspects of organic fouling of forward osmosis membranes, *J. Memb. Sci.*,

- 268 320(1–2), 292–302, doi:10.1016/j.memsci.2008.04.036, 2008.
- 269 Mohammadifakhr, M., de Groot, J., Roesink, H. D. W. and Kemperman, A. J. B.: Forward Osmosis: A Critical Review,
270 Processes, 8(4), 404, doi:10.3390/pr8040404, 2020.
- 271 Ong, R. C., Chung, T. S., Helmer, B. J. and De Wit, J. S.: Novel cellulose esters for forward osmosis membranes, Ind. Eng.
272 Chem. Res., 51(49), 16135–16145, doi:10.1021/ie302654h, 2012.
- 273 Peñate, B. and García-Rodríguez, L.: Current trends and future prospects in the design of seawater reverse osmosis
274 desalination technology, Desalination, 284(4), 1–8, doi:10.1016/j.desal.2011.09.010, 2012.
- 275 Raaijmakers, M. J. T. and Benes, N. E.: Current trends in interfacial polymerization chemistry, Prog. Polym. Sci., 63, 86–
276 142, doi:10.1016/j.progpolymsci.2016.06.004, 2016.
- 277 Ren, J. and McCutcheon, J. R.: A new commercial thin film composite membrane for forward osmosis, Desalination, 343,
278 187–193, doi:10.1016/j.desal.2013.11.026, 2014.
- 279 Ren, J. and McCutcheon, J. R.: Making Thin Film Composite Hollow Fiber Forward Osmosis Membranes at the Module
280 Scale Using Commercial Ultrafiltration Membranes, Ind. Eng. Chem. Res., 56(14), 4074–4082,
281 doi:10.1021/acs.iecr.6b04931, 2017.
- 282 Tian, M., Qiu, C., Liao, Y., Chou, S. and Wang, R.: Preparation of polyamide thin film composite forward osmosis
283 membranes using electrospun polyvinylidene fluoride (PVDF) nanofibers as substrates, Sep. Purif. Technol., 118, 727–736,
284 doi:10.1016/j.seppur.2013.08.021, 2013.
- 285 Vatanpour, V., Sheydaei, M. and Esmaeili, M.: Box-Behnken design as a systematic approach to inspect correlation between
286 synthesis conditions and desalination performance of TFC RO membranes, Desalination, 420(June), 1–11,
287 doi:10.1016/j.desal.2017.06.022, 2017.
- 288 Wang, Y., Guo, H., Xie, C., Zhou, N. and Fang, Z.: Study on the Influence of Interfacial Polymerization Process on Thin –
289 Film Composite (TFC) Forward Osmosis (FO) Membrane Synthesis, Chem. Eng. Trans., 59, 121–126,
290 doi:10.3303/CET1759021, 2017.
- 291 Xia, L., Andersen, M. F., Hélix-Nielsen, C. and McCutcheon, J. R.: Novel Commercial Aquaporin Flat-Sheet Membrane for
292 Forward Osmosis, Ind. Eng. Chem. Res., 56(41), 11919–11925, doi:10.1021/acs.iecr.7b02368, 2017.
- 293 Zhao, L., Chang, P. C. Y., Yen, C. and Ho, W. S. W.: High-flux and fouling-resistant membranes for brackish water
294 desalination, J. Memb. Sci., 425–426, 1–10, doi:10.1016/j.memsci.2012.09.018, 2013.
- 295 Zhao, S., Zou, L., Tang, C. Y. and Mulcahy, D.: Recent developments in forward osmosis : Opportunities and challenges, J.
296 Memb. Sci., 396, 1–21, doi:10.1016/j.memsci.2011.12.023, 2012.
- 297 Zhou, Z., Lee, J. Y. and Chung, T.-S.: Thin film composite forward-osmosis membranes with enhanced internal osmotic
298 pressure for internal concentration polarization reduction, Chem. Eng. J., 249, 236–245, doi:10.1016/j.cej.2014.03.049,
299 2014.
- 300