



Estimating fast and slow reacting components in surface water and groundwater using a two-reactant model

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Abstract. Maintaining residual chlorine levels in a water distribution network is a challenging task, especially in the context of developing countries where water is usually supplied intermittently. To model chlorine decay in water distribution networks, it is very important to understand chlorine kinetics in bulk water. Recent studies have suggested that chlorine decay rate depends on initial chlorine levels and the type of organic and inorganic matter present in water, indicating that a first-order decay model is unable to accurately predict chlorine decay in bulk water. In this study, we employed the two-reactant (2R) model to estimate the fast and slow reacting components in surface water and groundwater. We carried out a bench-scale test for surface water and groundwater at initial chlorine levels of 1, 2, and 5 mg L⁻¹. We used decay data sets to estimate optimal parameter values for both surface water and groundwater. After calibration, the 2R model was validated with two decay data sets with varying initial chlorine concentrations (ICCs). This study arrived at three important findings. (a) We found that the ratio of slow to fast reacting components in groundwater was 30 times greater than that of the surface water. This observation supports the existing literature which indicates the presence of high levels of slow reacting fractions (manganese and aromatic hydrocarbons) in groundwater. (b) Both for surface water and groundwater, we obtained good model prediction, explaining 97 % of the variance in data for all cases. The mean square error obtained for the decay data sets was close to the instrument error, indicating the feasibility of the 2R model for chlorine prediction in both types of water. (c) In the case of deep groundwater, for high ICC levels (> 2 mg L⁻¹), the first-order model can accurately predict chlorine decay in bulk water.

1 Introduction

The presence of 0.2 mg L⁻¹ of residual chlorine in drinking water is known to reduce public health risks significantly (Arnold and Colford, 2007; Pattanayak et al., 2005). One of the key tasks of water managers worldwide, especially in developing nations, is to maintain residual chlorine levels of drinking water in distribution systems. This requires a higher concentration at entry point in order to ensure that a minimal residual chlorine concentration of 0.2 mg L⁻¹ is retained at any point of time before reaching the end consumers.

To maintain 0.2 mg L⁻¹ of residual chlorine in water, sodium hypochlorite or liquid chlorine is added to the treated

water. Before water reaches the consumers, part of this chlorine is lost due to reactions with the organic and inorganic matter present in water after treatment, as well as to reactions with biofilms and corrosion products present within the distribution network (Al-Jasser, 2007; Hallam et al., 2002; Helbling and VanBriesen, 2007). Any excessive addition of chlorine to water leads to harmful by-products which pose risks to public health. Therefore it becomes very important for water managers to optimize the dose of chlorine added to water, ensuring that the right level of residual chlorine is retained in distribution networks (Hrudey, 2009; Richardson, 2003; Singer, 1999).

A first-order decay process is generally employed to simulate chlorine decay within the distribution network (Hua et al., 1999; Rossman et al., 1994; Vasconcelos et al., 1997). The model assumes that chlorine decay rate is a function of chlorine levels within the bulk water. However, recent studies have shown that in addition to chlorine levels, other factors like the type of organic/inorganic matter, temperature, and pipe material also affect chlorine decay rates in the distribution system (Al-Jasser, 2007; Mutoti et al., 2007; Hallam et al., 2002).

The total chlorine decay within the water distribution network is caused by chlorine reaction (a) in bulk water and (b) with the biofilm attached to the pipe surface, also termed wall decay (Al-Jasser, 2007; Hallam et al., 2002; Powell et al., 2000). For prediction of chlorine decay over time, models require accurate estimation of chlorine reaction in bulk water and with the biofilm on the pipe wall surface. Pilot loop setups/simulators are employed to estimate the contribution of wall reactions to chlorine decay (Frias et al., 2001; Lehtola et al., 2006; Rossman et al., 1994, 2006). This is achieved by subtracting the bulk reaction rate from the total chlorine decay rate in the pipe loop. Various authors have argued about the need to accurately model bulk decay before making an attempt to estimate the contribution of wall decay (Fisher et al., 2011).

Chlorine decay kinetics depends on the type and amount of dissolved organic matter (DOM) and inorganic matter present in bulk water. DOM is derived primarily from decaying organisms such as plants or algae, and is often classified into humic and non-humic substances such as proteins, carbohydrates, and lipids. Generally speaking, DOM from marine and aquatic sources is more enriched in aliphatic structures, while DOM from terrestrial/higher plant sources is rich in aromatic compounds (Chen et al., 2010). The inorganic compounds in surface water are derived from the dissolution of minerals present in the bedrock as water flows, whereas groundwater dissolves minerals as it percolates through the vadose zone as well as during its stay in the saturated zone. Therefore, in comparison to surface water, groundwater contains high levels of inorganic substances such as nitrates, manganese, arsenic, and iron.

Several studies have shown that in homogeneous systems, chlorine exhibits faster reaction rates with ammonia, sulfates, nitrates, nitrites, arsenic, and iron as compared to manganese (Mn (II)) (Deborde and Von Gunten, 2008). Therefore, given different characteristics of the components (organic and inorganic) present in surface water and groundwater, the precursors to chlorine reactions can be divided into fast and slow reacting fractions (Gallard and von Gunten, 2002). Table 1 presents the list of possible fast and slow reacting components in different types of water.

The two-reactant model (2R model) is a simplified second-order decay model which uses notional fast and slow reacting agents involved in second-order reactions with chlorine over long travel periods within the distribution network (Fisher et

Table 1. Fast and slow reacting components present in different types of water.

Compounds	Organic	Inorganic
Fast reacting	Aliphatic hydrocarbons	Nitrates, sulfates, ammonia, and nitrites
Slow reacting	Aromatic hydrocarbons	Manganese Mn (II)

al., 2011). The second-order reaction rates and the resulting 2R model are given by the following equations:

$$\frac{dC_f}{dt} = -K_f \cdot C_f \cdot C_{cl}, \quad (1)$$

$$\frac{dC_s}{dt} = -K_s \cdot C_s \cdot C_{cl}, \quad (2)$$

$$\frac{dC_{cl}}{dt} = \frac{dC_f}{dt} + \frac{dC_s}{dt}, \quad (3)$$

where C_{cl} is the concentration of residual chlorine levels (mg L^{-1}), C_f and C_s are the concentrations of fast and slow reducing agents (mg L^{-1}), and K_f and K_s are the fast and slow reaction rate coefficients ($\text{L mg}^{-1} \text{h}^{-1}$).

The initial concentration of fast and slow reactants (C_{of} and C_{os}) and their respective decay coefficients (K_s and K_f) can be estimated using the AQUASIM software (Fisher et al., 2011).

So far, first- and second-order chlorine decay models have been calibrated and tested for different types of test water under varying conditions such as temperature, type of treatment, and re-chlorination (Fisher et al., 2012; Mutoti et al., 2007; Rossman, 2006). All prior studies have estimated the chlorine decay parameters for water from different sources (variable water quality). The results obtained are specific and suitable for predicting chlorine decay in water supply networks of the source water for which the studies were conducted. This study aims to estimate the chlorine decay parameters using the 2R model relevant to local conditions found in southern India, where hard rock aquifers are abundant, and compare them with surface water parameters. We employed the 2R model to estimate optimal parameters for prediction of residual chlorine in both surface water and groundwater. The model was calibrated separately for test water with initial chlorine levels ranging from 1 to 5 mg L^{-1} . To establish the suitability of the 2R model, we also validated it against two chlorine decay data sets.

2 Methodology

We first calibrated the 2R model against data sets for two types of water, surface water and groundwater, to obtain a single invariant set of four parameters that characterize the water. The model was then validated by comparing the model estimates with the decay test data. The characteristics of the experimental data set are presented in Table 2.

Table 2. Characteristics of the data set.

Water	Treatment	ICC range (mg L ⁻¹)	Number of experimental runs	Temperature range (°C)
Surface water	Conventional treatment	1–5	4	25–30
Groundwater	No treatment	1–5	4	25–30

2.1 Chlorine decay data sets

Chlorine decay tests and data for calibration and validation of the 2R model were obtained by conducting bench-scale residual chlorine decay tests at the ATREE water and soil laboratory.

Groundwater and surface water samples were obtained from the respective sources and water quality characteristics were determined as presented in Table 3. The test water was stored in amber glass bottles, while sodium hypochlorite was added to attain the desired initial chlorine concentrations (ICCs). The bench-scale tests for both types of water were run at ICC-1, 2, 4.5, and 5 mg L⁻¹. The amber glass bottles were kept in an incubator set at ambient temperature (25 to 30 °C). During the day, hourly samples were drawn from the bottles and free chlorine levels were measured for 72 h. Free chlorine in the test water was measured using a Merck Spectroquant® Picco colorimeter. The free chlorine measurement range of the instrument is 0.05 to 6.00 mg L⁻¹ (APHA, 2005). The decay test results obtained were within the measurement range of the instrument.

2.2 Model parameter estimation

The AQUASIM software was used to estimate optimal parameter values for the 2R model to obtain the best fit for the three decay data sets (ICC-1, 2, and 5 mg L⁻¹; bench-scale laboratory experiments). Optimal parameters are the values that allow the model to predict chlorine decay in each type of water as accurately as possible. As explained by Fisher et al. (2012), the AQUASIM software calculates the sum of squared differences between each experimental data point and the corresponding model prediction, assuming an initial set of parameter values. This sum is derived by the variance of the data to form a chi square (χ^2). Using the simplex technique it then systematically varies the parameter values to search for a set that produces the best fit (minimizes χ^2). The coefficient of determination (R^2) was also obtained which indicates the total variance in the data set explained by the 2R model regardless of the distance between the decay curves. To measure the 2R model accuracy for chlorine prediction, we also estimated the root mean square error (RMSE) for the data sets.

We calibrated the 2R model using chlorine decay data sets for initial chlorine levels of 1, 2, and 5 mg L⁻¹. The optimal parameters for groundwater and surface water were determined separately. After calibration, the 2R model was val-

idated using two data sets, i.e. of ICC-2 mg L⁻¹ (a subset of the calibration data set) and ICC-4.5 mg L⁻¹ (independent chlorine decay data set).

3 Results

3.1 Chlorine decay and water quality

The results of bench-scale chlorine decay tests are presented in Fig. 1. The graph presents the fraction of chlorine remaining in test water at different ICCs. The data present two interesting findings: (i) the decay rate decreases with an increase in initial chlorine levels and (ii) the chlorine decay rate in surface water is greater than that of groundwater. The above results are in conjugation with the other studies that suggest that the first-order decay model is unable to predict chlorine decay in bulk water, and the chlorine decay rate depends on the ICC and level of organic/inorganic matter present in the test water (Fisher et al., 2011; Hua et al., 1999; Rossman, 2006).

As shown in Table 2, the ambient temperature during this study fluctuated between 25 and 30 °C. The temperature alone could not explain the variation in the first-order decay constant at different ICCs. Therefore we employed the 2R model to predict the chlorine decay in bulk water. As per the literature review, none of the earlier studies have used the 2R model to estimate fast and slow reacting components of groundwater from deep hard rock aquifers. Fisher et al. (2011) estimated decay parameters for shallow and deep groundwater from the Wanneroo aquifer (Fisher et al., 2015; Warton et al., 2006), which could not be applied as-is to predict chlorine decay in deep groundwater from hard rock aquifers. The decay parameter, estimated by the 2R model, depends on the quality of the source water. Therefore in this study, an attempt has been made to estimate decay parameters specific to the local water sources and conditions.

In the next section, we employ the 2R model to estimate fast and slow reacting components in test waters. In addition, we will also test the feasibility of the 2R model in predicting chlorine decay in test waters.

3.2 2R model calibration and validation

The 2R model for groundwater and surface water was calibrated separately using the data sets for ICC-1, 2, and 5 mg L⁻¹. Figure 2 presents the calibrated data sets for groundwater and surface water.

Table 3. Water quality parameters of test water.

Parameter	Surface water (<i>n</i> = 3)	Standard deviation	Groundwater (<i>n</i> = 3)	Standard deviation
pH	7.19	0.47	6.75	0.01
Conductivity ($\mu\text{S cm}^{-1}$)	434	30	1150	17
Nitrates (mg L^{-1})	3	1	177	20
Hardness (mg L^{-1})	180	56	352	8
Alkalinity (mg L^{-1})	196	4	165	3

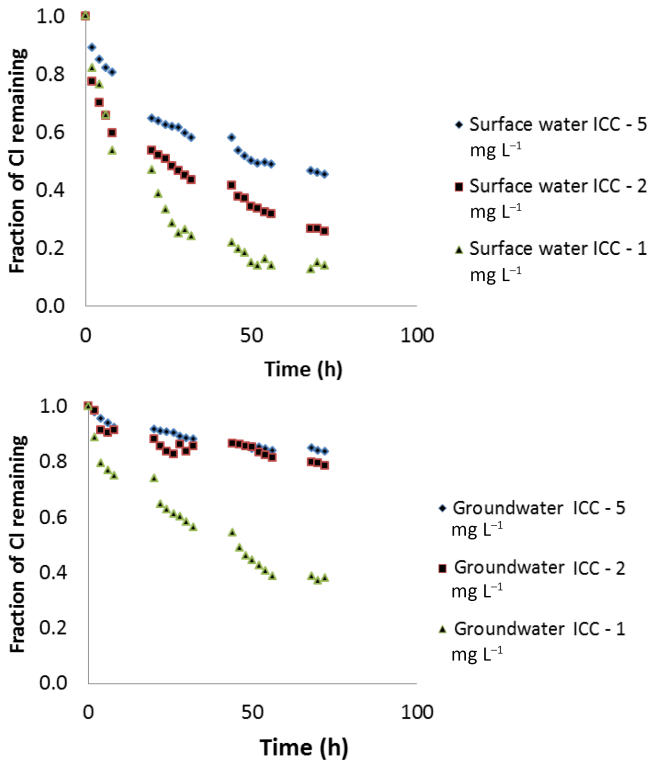


Figure 1. Fraction of chlorine remaining in surface water and groundwater at different initial chlorine levels.

The 2R model predicted optimal values for four parameters simultaneously by minimizing the chi-squared (χ^2) value. Minimization of χ^2 was readily achieved using the optimization technique available within the AQUASIM parameter estimation procedure. The optimal values with the associated χ^2 value are presented in Table 4.

Figure 2 presents the decay curves obtained from the simulation using optimized parameter values for the calibration data sets. We observed good agreement between chlorine residual data and the model estimates for all ICCs, both for surface water and groundwater.

The χ^2 values obtained for surface water and groundwater were 0.18 and 0.48, respectively. The R^2 values were greater than 0.98 for surface water and 0.99 for groundwater, indicating that only 2 and 1% variance in the calibra-

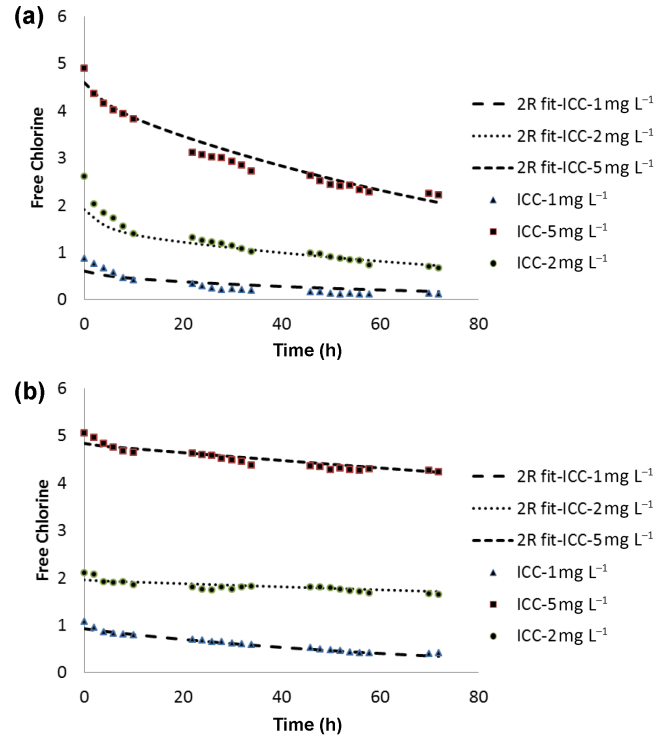


Figure 2. Chlorine decay in surface water (a) and groundwater (b): markers – measured chlorine values; curves – values simulated by 2R models.

tion data sets remained unexplained by the model. We also checked the validity of our results by comparing optimal parameter values obtained from our data sets with those of the other studies. Table 4 presents the optimal parameters obtained for other test waters. The χ^2 values obtained for our data sets were comparable to those of the experimental data sets from other studies (Fisher et al., 2012). For surface water, the 2R model underestimated chlorine levels for $0 < t < 60$ h for decay sets ICC-5 and ICC-1 mg L^{-1} , whereas for ICC-2 mg L^{-1} the chlorine levels were underestimated for $0 < t < 20$ h. In the case of groundwater, chlorine decay was underestimated for ICC-5 and ICC-2 mg L^{-1} for $0 < t < 60$ h, and for ICC-1 mg L^{-1} chlorine was underestimated for $0 < t < 5$ h.

Table 4. Comparison of optimal parameter values obtained for different test waters.

Source	Treatment type	ICC range (mg L ⁻¹)	C _{of} (mg L ⁻¹)	C _{os} (mg L ⁻¹)	K _f (L mg ⁻¹ h ⁻¹)	K _s (L mg ⁻¹ h ⁻¹)	C _{os} /C _{of}	χ ²	R ²
Surface water ¹	Conventional treatment	1–5	0.51	2.88	2.55	0.0069	6	0.18	0.978
Groundwater ¹	No treatment	1–5	0.003	0.67	8.07	0.013	223	0.48	0.998
Surface water ²	Conventional treatment	1–4	0.808	3.88	0.261	0.0102	5	0.18	0.992
Surface water ²	No treatment	1–4	0.761	2.69	0.199	0.0066	4	0.97	0.987
Surface water ²	Not known	1–4	0.917	1.98	6.18	0.085	2	0.844	0.987

¹ Bench-scale test (our study). ² Bench-scale test (Fisher et al., 2012).

In groundwater, the ratio of slow to fast reacting components was 30 times greater than that of the surface water. This suggests that, as groundwater travels through the vadose zone, most of the fast reacting organic matter is consumed by microorganisms, leaving behind the non-biodegradable organic/inorganic matter (slow reacting component) (He et al., 2006; McCarty et al., 1981). The slow reacting components are difficult to oxidize; therefore, over time, high levels of residual chlorine were observed in groundwater. It also suggests that in the absence of fast reacting components, first-order decay models could accurately predict chlorine decay in groundwater at ICCs greater than 2 mg L⁻¹.

3.3 Validation of the 2R model

The 2R model was fitted for experimental data sets – (a) surface water (ICC-2.6 and 4.2 mg L⁻¹) and (b) groundwater (ICC-2 and 4.5 mg L⁻¹), as shown in Fig. 3.

First we calibrated the 2R model with decay data sets, commencing with the highest and lowest ICCs, as the extrapolation outside the calibration range is less reliable. Then we validated the model by using two chlorine decay data sets, i.e. one from the calibration data set (ICC-2 mg L⁻¹) and one from the other data set that has not been used for the model calibration (ICC-4 mg L⁻¹).

The R² value obtained for both the data sets of surface water was greater than 0.98, indicating that only 2 % of the variance remains unexplained by the 2R model. This suggests the suitability of the 2R model for chlorine prediction in surface water. In the case of groundwater, R² values of 0.89 and 0.94 were obtained for decay tests at ICC-2 and ICC-4.5 mg L⁻¹, respectively. The reason for the lower R² values for the validated data for groundwater is that R² is a measure of fit involving the error relative to the variance in the data. The groundwater data have lower variance than surface water data and at lower ICC groundwater data have lower variance than the higher ICC data. Therefore, even with the same level of error in all data, the groundwater chlorine decay data sets showed low R² values as compared to the surface water chlorine decay data sets.

To check the prediction accuracy of the 2R model, we estimated the mean square error for both surface water and groundwater data sets. The values obtained were ±0.07 and

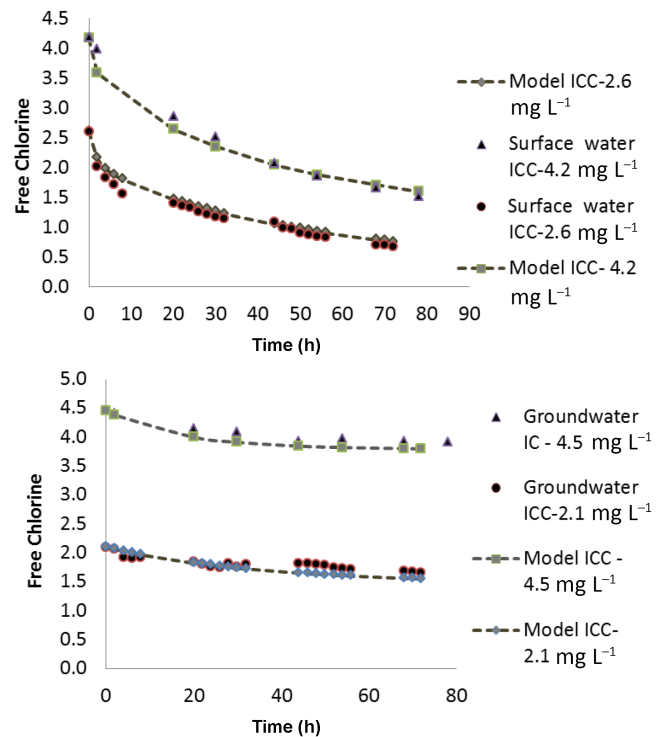


Figure 3. Validation of the 2R model for surface water and groundwater at different ICCs.

±0.05 mg L⁻¹ for surface water and groundwater, respectively, which is close to the instrument measurement error (±0.05 mg L⁻¹). This indicates that the parameter estimates obtained could accurately predict chlorine decay in surface water and groundwater.

4 Conclusions

Through this study, we estimated the fast and slow reacting components and tested the feasibility of the 2R model in predicting residual chlorine in bulk water from different sources, i.e. for surface water (rivers) and groundwater (deep aquifers). The 2R model was calibrated and validated using the AQUASIM software.

For both types of water, the observed chlorine residual values in bulk water closely matched the 2R model predicted values (ICC-1 to 5 mg L⁻¹). The 2R model calibration and validation range was well within the chlorine residual range encountered in water distribution networks (0–6 mg L⁻¹). Therefore, we can conclude with a reasonable degree of confidence that these invariant sets of model parameters obtained for surface water and groundwater if used in conjunction with the EPANET-MSX (Multi-Species extension) model will significantly assist public utilities in dealing with water quality issues in water distribution networks.

This study is also important in the context of urban areas in developing countries where 50 % of the water demand (Deccan plateau region – southern India) is met by groundwater pumping (Grönwall et al., 2010). The groundwater is pumped to overhead tanks, chlorinated, and supplied through a piped water connection. As stated above, the results of this study in conjunction with a sufficiently accurate prediction of wall decay will enable water management agencies to determine the ICC levels that allow residual targets at system extremities to be met.

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